

# Automatic Computing Methods for Special Functions.

## Part IV. Complex Error Function, Fresnel Integrals, and Other Related Functions

Irene A. Stegun\* and Ruth Zucker\*

National Bureau of Standards, Washington, DC 20234

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Accurate, efficient, automatic methods for computing the complex error function to any precision are detailed and implemented in an American Standard FORTRAN subroutine. A six significant figure table of  $\text{erf } z$ ,  $e^{z^2} \text{erfc } z$ , and  $e^{z^2} \text{erfc}(-z)$  is included for  $z$  in polar coordinate form with the modulus of  $z$  ranging from 0 to 9. The argand diagram is given for  $\text{erf } z$ .

Key words: Argand diagram; complex error function; continued fraction; Dawson's function; FORTRAN subroutine; Fresnel integrals; key values; line broadening function; plasma dispersion function; Voigt function.

### 1. Introduction

In computing many of the functions of mathematical physics, for example, Fresnel integrals, Dawson's integral, Voigt function, plasma dispersion function, etc., difficulties are frequently encountered. Since these functions may be expressed in terms of the error function of complex argument, we have chosen this function for Part IV.<sup>1</sup> The major part of the coding of the power series, continued fraction and asymptotic expansion computations for complex arguments will carry over equally well for other functions.

As Part I was devoted to the error function of a real variable, the probability function and other related functions, Part IV will only emphasize those functions and pitfalls due to complex arguments.

While accuracy over the entire domain of definition remains our main concern, the methods employed ensure efficiency, portability and ease of programming and modification.

If one supplies approximate values for the maximum machine value, minimum machine value, the upper bound of the sine, cosine routine, and the upper bound to the acceptable relative error and gives the square root of  $\pi$  to the required number of significant figures, the detailed methods will work for computations ranging from very low precision to multi-precision.

The argand diagram of  $\text{erf } z$  is included as well as the implementing ANS FORTRAN program and a six significant figure table of  $\text{erfc } z$ ,  $e^{z^2} \text{erfc } z$  and  $e^{z^2} \text{erfc}(-z)$  for  $z$  in polar coordinate form with the modulus of  $z$  ranging from 0 to 9.

### 2. Mathematical properties

Relevant formulas are collected here for completeness and ease of reference. In keeping with the convention of the Handbook [1],<sup>2</sup>  $z = x + i y$  is a complex variable.

\*Mathematical Analysis Division, Center for Applied Mathematics.

<sup>1</sup> Part I. Error, Probability, and Related Functions. J. Res. Nat. Bur. Stand. (U.S.), 74(3): 211–224; 1970. Part II. The Exponential Integral  $E_n(x)$ . J. Res. Nat. Bur. Stand. (U.S.), 78(4): 199–216; 1974. Part III. The Sine, Cosine, Exponential Integrals, and Related Functions. J. Res. Nat. Bur. Stand. (U.S.), 80(2): 291–311; 1976.

<sup>2</sup> Figures in brackets indicate literature references at the end of this paper.

## A. Definitions

$$\operatorname{erf} z = \frac{2}{\sqrt{\pi}} \int_0^z e^{-t^2} dt$$

$$\operatorname{erfc} z = \frac{2}{\sqrt{\pi}} \int_z^\infty e^{-t^2} dt = 1 - \operatorname{erf} z$$

(The path of integration is subject to the restriction  $\arg t \rightarrow \alpha$  with  $|\alpha| < \frac{\pi}{4}$  as  $t \rightarrow \infty$  along the path. If  $Rt^2$  remains bounded to the left,  $\alpha = \frac{\pi}{4}$  is permissible.)

$$\begin{aligned} w(z) &= e^{-z^2} (1 + \frac{2i}{\sqrt{\pi}} \int_0^z e^{t^2} dt) = e^{-z^2} \operatorname{erfc}(-iz) = e^{z^2} \operatorname{erfc}\xi (\xi = -iz) \\ &= \frac{i}{\pi} \int_{-\infty}^{\infty} \frac{e^{-t^2} dt}{z-t} = \frac{2iz}{\pi} \int_0^{\infty} \frac{e^{-t^2} dt}{z^2 - t^2} (I z > 0) \end{aligned}$$

with  $F(z) = e^{-z^2} \int_0^z e^{t^2} dt$  (Dawson's Function)

and  $Z(z) = \frac{1}{\sqrt{\pi}} \int_{-\infty}^{\infty} \frac{e^{-t^2} dt}{t-z}$  (Plasma Dispersion Function)

$$\begin{aligned} E(z) &= C(z) + i S(z) = \int_0^z e^{ix^{3/2}} dt = \int_0^z \cos(\frac{\pi t^2}{2}) dt + i \int_0^z \sin(\frac{\pi t^2}{2}) dt \\ &= \frac{1+i}{2} \operatorname{erf}[\frac{\sqrt{\pi}}{2}(1-i)z] \quad (\text{Fresnel Functions}) \end{aligned}$$

$$W(x,t) = \frac{\omega}{(4\pi t)^{1/2}} \int_{-\infty}^{\infty} \frac{e^{-u^2} du}{u^2 + \omega^2} = (-\frac{\pi}{4t})^{1/2} e^{\omega^2} \operatorname{erfc} \omega$$

where

$$\omega = (1-ix)/2 t^{1/2}$$

$= U(x,t) + i V(x,t)$  (Voigt Function)

$$= \frac{1}{(4\pi t)^{1/2}} \int_{-\infty}^{\infty} \frac{e^{-(x-y)^2/4t}}{1+y^2} dy + \frac{i}{(4\pi t)^{1/2}} \int_{-\infty}^{\infty} \frac{ye^{-(x-y)^2/4t}}{1+y^2} dy$$

$$H(a,u) = \frac{a}{\pi} \int_{-\infty}^{\infty} \frac{e^{-t^2} dt}{(u-t)^2 + a^2} = \frac{1}{a\sqrt{\pi}} U(u/a, 1/4a^2) \quad (\text{Line Broadening Function})$$

## B. Series Expansions

$$\operatorname{erf} z = \frac{2}{\sqrt{\pi}} \sum_{n=0}^{\infty} \frac{(-1)^n z^{2n+1}}{n! (2n+1)}$$

$$= \frac{2}{\sqrt{\pi}} e^{-z^2} \sum_{n=0}^{\infty} \frac{2^n z^{2n+1}}{1 \cdot 3 \cdots (2n+1)}$$

## C. Continued Fraction ( $Rz > 0$ )

$$\begin{aligned} e^{z^2} \operatorname{erfc} z &= \frac{1}{\sqrt{\pi}} \left[ \frac{1}{z+} \frac{1/2}{z+} \frac{1}{z+} \frac{3/2}{z+} \frac{2}{z+} \dots \right] \\ &= \frac{2z}{\sqrt{\pi}} \left[ \frac{1}{2z^2+1} - \frac{1 \cdot 2}{2z^2+5} - \frac{3 \cdot 4}{2z^2+9} - \dots \right] \quad (\text{"Even" Form}) \end{aligned}$$

## D. Asymptotic Expansion

$$e^{-z^2} \operatorname{erfc} z \sim \frac{1}{\sqrt{\pi}} \left[ \frac{1}{z} + \sum_{n=1}^{\infty} \frac{(-1)^n 1 \cdot 3 \cdots (2n-1)}{z (2z^2)^n} \right] (z \rightarrow \infty, |\arg z| < \frac{3\pi}{4})$$

## E. Symmetry Relations

$$\operatorname{erf}(-z) = -\operatorname{erf}z$$

$$\operatorname{erf}\bar{z} = \overline{\operatorname{erf}z}$$

$$w(-z) = 2e^{-z^2} - w(z)$$

$$\overline{w(z)} = \overline{w(-z)}$$

$$C(-z) = -C(z), S(-z) = -S(z)$$

$$C(iz) = i C(z), S(iz) = -i S(z)$$

$$\overline{C(z)} = \overline{C(\bar{z})}, \overline{S(z)} = \overline{S(\bar{z})}$$

## 3. Method

The main functions under consideration are the error function ERFZ, the complementary error function ERFCZ, and the exponential of  $z^2$  times the complementary error function EZ2CZ. All other functions may be obtained from these three. To simplify testing, computations are performed for  $z$  in the first quadrant AZ and symmetry relations are then employed to make adjustments for other quadrants. For the special case  $z = 0$ , no computations are performed and the following function values are returned: ERFZ = 0, ERFCZ = 1 and EZ2CZ = 1.

Real type variables are used throughout to readily allow for double precision computation if greater accuracy is needed. The machine dependent constants are placed in a labeled section at the beginning of the subroutine. Function references are likewise grouped together when possible and attention called to the statement labels of the remaining function references. Real and imaginary parts of complex variables have R and I as final characters.

Since EZ2CZ for  $z$  in the first quadrant is machine representable even with the real and imaginary parts of  $z$  equal to the maximum machine value CMAX (provided its reciprocal is larger than the minimum machine value CMIN), checking for the range of the argument  $z$  has been omitted. However, the extensive range necessitates a fair amount of testing for overflows. Underflows are assumed to be set to zero. Overflows are set equal to the maximum machine value and an error indicator IERR set for the number of functions affected. If only EZ2CZ lies outside the machine range, IERR = 1, otherwise IERR = 3. As often as possible, computations are arranged so as to give the correct results for the three functions if they lie within the range of the machine.

In computing the modulus RHO =  $\sqrt{(AZR)^2 + (AZI)^2}$  of a complex quantity AZ = AZR + i AZI in the first quadrant, RHO may lie in the machine range but  $(AZR)^2, (AZI)^2$  or their sum may be outside the range. We select the larger ARIMX and smaller ARIMN of either AZR or AZI, and compute the ratio RMNMX = ARIMN/ARIMX. A factor of RHO called PRHO is computed as the square root of  $(RMNMX * RMNMX + ONE)$ . This factor, which is greater than or equal to one and less than or equal to the square root of 2, can then be used to check for overflow. The quantity ARIMX must be less than CMAX divided by PRHO for RHO to lie in the machine range. A similar procedure is followed in computing the real and imaginary parts of  $(AZ)^2 = Z2R + i AZ2I = (AZR)^2 - (AZI)^2 + i 2AZR * AZI$  with first checking to ensure ARIMX is greater than or equal to 1.

Analysis has indicated and testing confirmed that the power series PS is most useful from the standpoint of accuracy and efficiency for RHO less than RHOLS (= 1.5) and when AZR is less than or equal to 1 provid-

ed RHO is less than AELL ( $=\sqrt{-1n(TOLER)}$ ) where TOLER is the upper limit for the relative error. The continued fraction expansion CF is most useful for AZR greater than 1 and RHO greater than or equal to RHOLS. The asymptotic expansion AE is most useful for AZR less than or equal to 1 for RHO greater than or equal to AELL. For RHO greater than or equal to RHOLC ( $=\sqrt{0.5/TOLER}$ ) a rearrangement of arithmetic operations for the first term of the asymptotic expansion is necessary to maintain the accuracy of EZ2CZ. In the continued fraction and asymptotic expansion regions only, EZ2CZ is first computed; it tends to zero for large  $|z|$  and the exponential of  $-z^2$  tends to infinity for small AZR. To maintain accuracy here, we compute the exponential of  $-Z2R/6$  and do continuous multiplication and testing with appropriate factors to obtain ERFC. The imaginary part of  $(AZ)^2$  is tested against ULSC, the upper limit of the sine, cosine routine.

Figure 1 below maps the regions for the various methods.

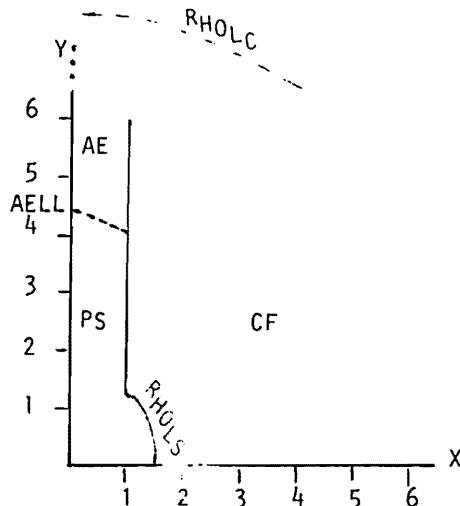


FIGURE 1. Parameter plane.

The dividing line  $RHO = AELL$  between the use of the power series and the asymptotic expansion and  $RHO = RHOLC$  are the only boundaries subject to the required precision. Single and double precision results, for example on the Univac 1108, are the results of two different methods in the region where RHO roughly lies between 4.3 and 6.4.

This mapping of the region ensures for the required precision that the least number of terms are computed and the loss of significance is kept to a minimum. While the second form of the power series is preferable for real positive  $z$ , since all terms are positive, the first form ensures greater accuracy for complex  $z$  since the real and imaginary parts of the terms may be positive, negative or zero for any RN( $=n$ ). The power series is there more rapidly convergent; the relative error may then be approximated by the ratio of the term to the sum of terms; comparison of this approximant with the tolerance for the relative error controls the number of terms needed. Since the terms tend to zero through underflow, there will always be convergence even if the tolerance is made considerably smaller than the precision of the machine. The power series is evaluated using recurrence relations in the following form:

$$ERFZ = \frac{\text{TWO}}{\text{SQRT(PI)}} \sum_{RN=0}^{RNF} SGN(RN) * TM(RN) = \frac{\text{TWO}}{\text{RTPI}} * \text{SUM}$$

where

$$SGN(0) = 1, SGN(RN + 1) = -SGN(RN)$$

$$TM(RN) = ((AZ^{**}(2*RN + 1))/1*2* \dots RN)/(2*RN + 1)$$

$$TM(RN) = PTM(RN)/DN(RN)$$

$$PTM(0) = AZ, PTM(RN + 1) = (AZ^{**}2)*PTM(RN)/(RN + 1)$$

$$DN(0) = 1, DN(RN + 1) = DN(RN) + 2$$

In determining the terminal value of RN, normalization is necessary to avoid overflows and underflows. The normalization factor TMAX is the maximum of the absolute value of the real and imaginary parts of TM and SUM. If TMAX equals zero or  $|TM/TMAX|^2$  underflows, RNF = RN.

If  $|SUM/TMAX|^2$  underflows, additional terms are obtained. Otherwise, if  $|TM/TMAX|^2/|SUM/TMAX|^2$  is less than TOLER<sup>2</sup>, then RNF = RN.

The continued fraction expansion starts to converge more slowly as z tends to zero. The "even" form is used since the required number of terms is halved at the expense of very little extra computation for successive numerators and denominators. The continued fraction is evaluated by using the recurrence relations in the "forward" direction. The number of terms needed is determined by checking to see if the relative error of two successive convergents is less than the tolerance. On the other hand, if the relative error remains constant or starts to increase, the recurrence is terminated and the prior convergent taken as the value of the continued fraction. In this way, the process is always terminated when maximum precision is attained.

The "even" form of the continued fraction takes on the following implementation:

$$EZ2CZ = \frac{2*AZ}{RTPI} \prod_{RN=1}^{RNF} \frac{AM(RN)}{BM(RN)}$$

with

$$AM(1) = 1, AM(RN + 1) = -WM(RN + 1)*(WM(RN + 1) + 1)$$

$$BM(1) = 2*(AZ**2) + 1, BM(RN + 1) = BM(RN) + 4$$

where

$$WM(1) = -1, WM(RN + 1) = WM(RN) + 2$$

$$EZ2CZ = (AZ*(FM/GM))*2/RTPI = (AZ*F(RN))*2/RTPI$$

where

$$FM(-1) = 1, FM(0) = 0$$

$$GM(-1) = 0, GM(0) = 1$$

and

$$FM(RN) = BM(RN)*FM(RN - 1) + AM(RN)*FM(RN - 2)$$

$$GM(RN) = BM(RN)*GM(RN - 1) + AM(RN)*GM(RN - 2)$$

The relative error may be approximated by  $[F(RN) - F(RN - 1)]/F(RN) = RE(RN)$ . If the modulus squared of the relative error REM2(RN) is less than the square of the tolerance divided by 8, RNF = RN. If REM2(RN) is greater than or equal to REM2(RN - 1), then RNF = RN - 1. Normalization is likewise necessary here to avoid overflows in computing the relative error and its modulus squared and also in the generation of the successive convergents.

The asymptotic expansion is likewise evaluated using recurrence relations in the following form:

$$EZ2CZ = \frac{1}{SQRT(Pi)} \sum_{RN=0}^{RNF} SGN(RN)*TM(RN) = SUM/RTPI$$

where

$$SGN(0) = 1, SGN(RN + 1) = -SGN(RN)$$

$$TM(RN) = (1/AZ)*(1*3* \dots * (2*RN - 1))/(2*(AZ**2)**RN$$

$$TM(0) = 1/AZ, TM(RN + 1) = DN(RN + 1)* TM(RN)*(1/(2*(AZ**2)))$$

with

$$DN(1) = 1, DN(RN + 1) = DN(RN) + 2.$$

The relative error may be approximated here by the ratio TM/SUM. The convergence test precedes the divergence test and is implemented as REM2 less than (TOLER\*\*2)/8 to attain greater accuracy in both the real and imaginary parts. If the modulus squared of the term remains the same or increases, the prior sum is taken as the final sum.

For  $z$  along the imaginary axis, the error function is purely imaginary; the real part of  $\text{erfc } z = 1$  and of  $e^{-z^2} \text{erfc } z = e^{-(AZI)^2}$ . No difficulties arise in the use of the power series. However, since the asymptotic expansion is given for  $|z| - \infty$ , the correction must be applied for  $AZR - 0$ .

The following table gives an indication of the number of terms needed to obtain maximum machine accuracy on the Univac 1108 with the various methods of computation.

Method	Number of Terms	
	Single Precision TOLER = .745E-8	Double Precision TOLER = .867D-18
Power Series	50	112
Continued Fraction	25	99
Asymptotic Expansion	22	45

#### 4. Range

If the real part of  $z$  is zero or positive,  $e^{-z^2} \text{erfc } z$  is valid for  $z$  throughout the entire machine range. Otherwise, the real part of  $z^2$  is essentially limited by the range of the exponential library subroutine with the imaginary part of  $z^2$  limited by the range of the sine, cosine library subroutine.

#### 5. Accuracy and Precision

The maximum relative error, generally in  $\text{erfc } z$ , except for regions in the immediate neighborhood of zeros of the real and/or imaginary parts of the functions is 8E-6 for single precision computation on the Univac 1108.

The precision may be varied by changing the value of TOLER.

#### 6. Timing (Univac 1108 Time/Sharing Executive System)

The time estimates given below are highly dependent on the operating system environment and consequently should not be relied on for critical timing measurements.

Region ZR = 0(.1)4, ZI = 0(.2)8 (1681 values)	Time (Seconds)	
	Single Precision TOLER = .745E-8	Double Precision TOLER = .867D-18
Method	5.94	22.5
	Maximum Time/Evaluation	
Power Series	.0101	.038
Continued Fraction	.0088	.052
Asymptotic Expansion	.0035	.0093

#### 7. Testing

The language of the subroutine was checked for conformity with the PPORT VERIFIER.<sup>3</sup> Test arguments were devised and used in the analysis of the subroutine with the PROFILER.<sup>4</sup>

<sup>3</sup> The PPORT Verifier, A. D. Hall and B. G. Ryder, Bell Laboratories, Murray Hill, N.J. Proceedings of the Computer Science and Statistics Eighth Annual Symposium on the Interface, University of California, Los Angeles, February 13-14, 1975.

<sup>4</sup> Program Execution Profiles, G. Sande, World Bank, Washington, D.C. Proceedings of the Computer Science and Statistics Eighth Annual Symposium on the Interface, University of California, Los Angeles, February 13-14, 1975.

The subroutine was used to obtain related functions which were checked against available published tables ([1]-[5], [7]-[9], [13], [15]). Single precision results covering the  $9 \times 9$  grid were compared against double precision results. This precision test particularly verified that the scaling operations were valid and undetected overflows had not occurred.

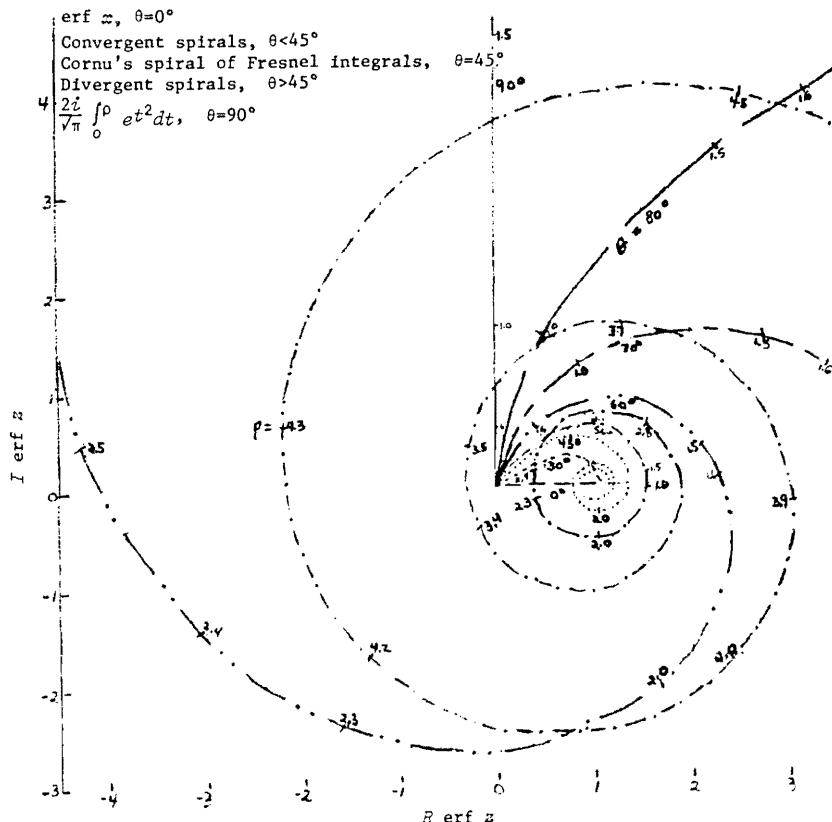
Where applicable, results were obtained by independent methods, for example, the power series and continued fraction, the power series and asymptotic expansion or all three methods. Otherwise, both forms of the power series or continued fraction were used. In addition, numerical integration of various forms of the integral representation was employed.

## 8. Test Values

Six-significant figure tables of  $\text{erfc } z$ ,  $e^{z^2} \text{erfc } z$  and  $e^{z^2} \text{erfc}(-z)$  are included in the appendix. The computations were performed with double precision arithmetic to provide more accurate values for checking purposes. The arguments are in polar coordinate form  $z = \rho e^{i\theta}$  for  $\rho = 0(0.02)2(1)3(5)9$ ,  $\Theta = 0^\circ(15^\circ)30^\circ, 37.5^\circ, 45^\circ, 50^\circ(10^\circ)90^\circ$ . Values of the functions for  $z$  in other quadrants are readily obtainable with symmetry relations.

$$9. \text{ Argand Diagram of } \text{erf } z = \frac{2}{\sqrt{\pi}} \int_0^{z=\rho e^{i\theta}} e^{-t^2} dt$$

Since  $\text{erf } z$  and  $\text{erfc } z$  are complementary functions,  $\text{erf } z$  is not tabulated but the argand diagram of the function is included to illustrate divergent and convergent spirals.



## 10. Special Values

Relevant values are collected here for completeness and ease of modification and checking of the program.

### Zeros

$$\operatorname{erf} z_s = 0$$

<i>s</i>	<i>z<sub>s</sub></i>
1	1.45061616 + i 1.88094300
2	2.24465927 + i 2.61657514
3	2.83974105 + i 3.17562810

$$w(z_s) = 0$$

<i>s</i>	<i>z<sub>s</sub></i>
1	1.99146684 - i 1.35481013
2	2.69114902 - i 2.17704491
3	3.23533087 - i 2.78438761

$$C(z_s) = 0$$

$$S(z_s) = 0$$

<i>s</i>	<i>z<sub>s</sub></i>	<i>z<sub>s</sub></i>
1	1.7437 + i .3057	2.0093 + i .2885
2	2.6515 + i .2529	2.8335 + i .2443
3	3.3204 + i .2240	3.4675 + i .2185

### Maxima and Minima of Fresnel Integrals

<i>s</i>	$M_s = C(\sqrt{4s+1})$	$m_s = C(\sqrt{4s+3})$	$M_s^* = S(\sqrt{4s+2})$	$m_s^* = S(\sqrt{4s+4})$
0	.779893	.321056	.713972	.343416
1	.640807	.380391	.628940	.387969
2	.605721	.404261	.600362	.408301
3	.588128	.417922	.584942	.420516

### Radius of Univalence $\varrho$

$$\int_0^{\varrho} e^{-t^2} dt = e^{-\varrho^2} \int_0^{\varrho} e^{-t^2} dt$$

$$\varrho = 1.5748376 \quad 92413887$$

### Maximum and Inflection Point for Dawson's Integral

$$F(.92413 \ 88730) = .54104 \ 42246$$

$$F(1.50197 \ 52682) = .42768 \ 66160$$

## Related Constants

$1^\circ$	=	1.74532 92519 94329 57692 36907 68488 61271 (-2)r
$\pi$	=	3.14159 26535 89793 23846 26433 83279 50288
$\pi/2$	=	1.57079 63267 94896 61923 13216 91639 75144
$\sqrt{\pi}$	=	1.77245 38509 05516 02729 81674 83341 14518
$\sqrt{\pi}/2$	=	.88622 69254 52758 01364 90837 41670 57259
$2\pi$	=	6.28318 53071 79586 47692 52867 66559 00576
$2/\sqrt{\pi}$	=	3.54490 77018 11032 05459 63349 66682 29036
$e$	=	2.71828 18284 59045 23536 02874 71352 66249
$1/\pi$	=	.31830 98861 83790 67153 77675 26745 02872
$2/\pi$	=	.63661 97723 67581 34307 55350 53490 05744
$1/\sqrt{\pi}$	=	.56418 95835 47756 28694 80794 51560 77258
$2/\sqrt{\pi}$	=	1.12837 91670 95512 57389 61589 03121 54517
$1/2\pi$	=	.15915 49430 91895 33576 88837 63372 51436
$1/2\sqrt{\pi}$	=	.28209 47917 73878 14347 40397 25780 38629
$1/e$	=	.36787 94411 71442 32159 55237 70161 46086
$\text{erf } 1$	=	.84270 07929 49714 86934 12206 35082 60926

$$\int_0^1 e^{-t^2} dt = (\sqrt{\pi}/2) \text{erf } 1 = \sum_{n=0}^{\infty} \frac{(-1)^n}{n!(2n+1)} = .74682 41328 12427 02539 94674 36131 85300$$

$$(\sqrt{\pi}/2)e^1 \text{erf } 1 = \sum_{n=0}^{\infty} \frac{2^n}{1 \cdot 3 \cdots (2n+1)} = 2.03007 84692 78704 97553 90899 25665 95044$$

$$\int_0^1 e^{t^2} dt = \sum_{n=0}^{\infty} \frac{1}{n!(2n+1)} = 1.46265 17459 07181 60880 40485 86856 98815$$

$$\sum_{n=0}^{\infty} \frac{1}{(2n)!(4n+1)} = 1.10473 79393 59804 31710 17580 11494 42058$$

$$\sum_{n=0}^{\infty} \frac{1}{(2n+1)!(4n+3)} = .35791 38065 47377 29170 22905 75362 56757$$

$$\sum_{n=0}^{\infty} \frac{2^{2n}}{1 \cdot 3 \cdots (4n+1)} = 1.28407 89880 95736 69733 77386 73036 75360$$

$$\sum_{n=0}^{\infty} \frac{2^{2n+1}}{1 \cdot 3 \cdots (4n+3)} = .74599 94811 82968 27820 13512 52629 19684$$

$$e^{-1} \int_0^1 e^{t^2} dt = \sum_{n=0}^{\infty} \frac{(-1)^n 2^n}{1 \cdot 3 \cdots (2n+1)} = .53807 95069 12768 41913 63874 20407 55675$$

## Typical Tolerances and Their Natural Logarithms

$2^{-16}$	=	0.15258 78906 25(-4)
$2^{-24}$	=	.59604 64477 53906 25(-7)
$2^{-27}$	=	.74505 80596 92382 8125(-8)
$2^{-36}$	=	.14551 91522 83668 51806 64062 5(-10)
$2^{-48}$	=	.35527 13678 80050 09293 55621 33789 0625(-14)
$2^{-56}$	=	.13877 78780 78144 56755 29539 58511 35253 90625(-16)
$2^{-60}$	=	.86736 17379 88403 54720 59622 40695 95336 91406 25(-18)
$2^{-108}$	=	.30814 87911 01957 73648 89564 70813 58837 09660 96263 71446 21112 38390 20729 06494 14062 5(-32)

$$\log_e(2^{-16}) = -11.09035 48889 59124 95067 57139 43330 82508$$

$$\log_e(2^{-24}) = -16.63553 23334 38687 42601 35709 14996 23763$$

$$\log_e(2^{-27}) = -18.71497 38751 18523 35426 52672 79370 76733$$

$\log_e(2^{-36}) = -24.95329$  85001 58031 13902 03563 72494 35645  
 $\log_e(2^{-45}) = -33.27106$  46668 77374 85202 71418 29992 47526  
 $\log_e(2^{-56}) = -38.81624$  21113 56937 32736 49988 01657 88781  
 $\log_e(2^{-60}) = -41.58883$  08335 96718 56503 39272 87490 59408  
 $\log_e(2^{-108}) = -74.85989$  55004 74093 41706 10691 17483 06935

Maximum and Minimum Machine Values and Their Natural Logarithms  
(Univac 1108 Single and Double Precision Limits)

NBC=Number of binary digits in the (biased) characteristic of a floating point number

$$2^{-(2^{NBC-1}+1)} \leq x < 2^{2^{NBC-1}-1}$$

NBC = 8

$2^{127} = 0.17014$  11834 60469 23173 16873 03715 88410(39)  
 $2^{-129} = .14693$  67938 52785 93849 60920 67152 78070(-38)  
 $\log_e(2^{127}) = 88.02969$  19311 13054 29598 84794 25188 42414  
 $\log_e(2^{-129}) = -89.41598$  62922 32944 91482 29436 68104 77728

NBC = 11

$2^{1023} = 0.89884$  65674 31157 95386 46525 95394 51236(308)  
 $2^{-1025} = .27813$  42323 13400 17288 62790 89666 55050(-308)  
 $\log_e(2^{1023}) = 709.08956$  57128 24051 53382 84602 51714 62914  
 $\log_e(2^{-1025}) = -710.47586$  00739 43942 15266 29244 94630 98227

## 11. References

- [1] Abramowitz, M. and Stegun, I. A. Handbook of Mathematical Functions. Nat. Bur. Stand. (U.S.) Appl. Math. Ser. 55; 1964.
- [2] Faddeeva, V. N. and Terent'ev, N. M. *Tables of Values of the Function  $w(z) = e^{-z^2}[1 + (2i/\sqrt{\pi}) \int_0^z e^{t^2} dt]$  for Complex Arguments.* New York: English Trans., Pergamon Press; 1961.
- [3] Fettis, H. E., Caslin J. C. and Cramer, K. R. Complex Zeros of the Error Function and of the Complementary Error Function. Math. Comp. **27**, 122: 401-407; 1973.
- [4] Finn, G. D. and Muggleton, D. Tables of the Line Broadening Function  $H(a,y)$ . Mon. Not. R. Astr. Soc. **129**: 221-235; 1965.
- [5] Fried, B. D. and Conte, S. D. *The Plasma Dispersion Function, The Hilbert Transform of the Gaussian.* New York: Academic Press; 1961.
- [6] Gautschi, W. Efficient Computation of the Complex Error Function. SIAM J. Numer. Anal. **7**, 1: 187-198; 1970.
- [7] Hummer, D. G. The Voigt Function: An Eight-Significant Figure Table and Generating Procedure. Mem. Roy. Astronom. Soc. **70**: 1-31, 1965.
- [8] Karpov, K. A. Tablitsy Funktsii  $w(z) = e^{-z^2} \int_0^z e^{t^2} dt$  v Kompleksnoi Oblasti. Moscow, U.S.S.R.: Izdat. Akad. Nauk S.S.S.R.; 1954.
- [9] Karpov, K. A. Tablitsy Funktsii  $F(z) = \int_0^z e^{-t^2} dt$  v Kompleksnoi Oblasti. Moscow, U.S.S.R.: Izdat. Akad. Nauk S.S.S.R.; 1958.
- [10] Kreyszig, E. and Todd, J. The Radius of Univalence of the Error Function. Numerische Mathematik **1**: 78-89; 1959.
- [11] Kreyszig, E. and Todd, J. On the Radius of Univalence of the Function  $\exp z^2 \int_0^z \exp(-t^2) dt$ . Pacific Journal of Mathematics **9**, 1: 123-127; 1959.
- [12] Lohmander, B. and Rittsten, S. Table of the Function  $y = e^{-z^2} \int_0^z e^{t^2} dt$ . Kungl. Fysiogr. Sällsk. i Lund Forh. **28**: 45-52; 1958.
- [13] Martz, C. W. Tables of the Complex Fresnel Integral. NASA Report SP-3010; Washington; 1964.
- [14] Pearcey, T. Table of the Fresnel Integral. London, England: Cambridge University Press; 1956.
- [15] Rosser, J. B. *Theory and Application of  $\int_0^z e^{-t^2} dt$  and  $\int_0^z e^{-p^2 t^2} dy \int_0^z e^{-t^2} dx$ .* Brooklyn, NY: Mapleton House; 1948.
- [16] Tablitsy Integralov Frenelya. Moscow, U.S.S.R.: Izdat. Akad. Nauk S.S.S.R.; 1953.
- [17] Van Wijngaarden, A. and Scheen, W. L., Table of Fresnel Integrals. Verh. Nederl. Akad. Wetensch. Afd. Natuurk. Sec. I, **19**, 4: 1-26; 1949.

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1      *****
2      APPENDIX
3      IMPLEMENTING PROGRAM
4      C LANGUAGE. AMERICAN NATIONAL STANDARD FORTRAN
5      C (SUBROUTINE SUBJECT TO PPORT VERIFIER*)
6      C DEFINITION. Z, A COMPLEX VARIABLE=ZR+I ZI
7      C      ERF(Z)=(2/SQRT(PI))*INTEGRAL(EXP(-T**2))DT FROM 0 TO Z
8      C      =ERFZR+I ERFZI
9      C      ERFC(Z)=(2/SQRT(PI))*INTEGRAL(EXP(-T**2))DT FROM Z TO
10     C                           INFINITY
11     C      =1-ERF(Z)
12     C      =ERFCZR+I ERFCZI
13     C      EXP(Z**2)*ERFC(Z)=EZ2CZR+I EZ2CZI
14     C      SYMMETRY RELATIONS
15     C      ERF(-Z)=-ERF(Z)
16     C      ERF(Z CCNJG)=(CCNJG(ERF(Z))
17     C      ERFC(-Z)=2-ERFC(Z)
18     C      ERFC(Z CONJG)=CCNJG(ERFC(Z))
19     C      EXP(Z**2)*ERFC(-Z)=2*EXP(Z**2)-EXP(Z**2)*ERFC(Z)
20     C      EXP(Z CCNJG**2)*ERFC(Z CONJG)=CCNJG(EXP(Z**2)*ERFC(Z))
21     C      SPECIAL CASE, Z=0
22     C      ERF(Z)=0
23     C      ERFC(Z)=1
24     C      EXP(Z**2)*ERFC(Z)=1
25     C      USAGE. CALL ERFZ (ZR,ZI,ERFZR,ERFZI,ERFCZR,ERFCZI,EZ2CZR,
26     C                           EZ2CZI,IERR)
27     C      ARGUMENTS
28     C      (REAL TYPE VARIABLES ARE USED THROUGHOUT TO READILY
29     C      ALLOW FOR DOUBLE PRECISION COMPUTATION. REAL AND
30     C      IMAGINARY PARTS OF COMPLEX VARIABLES HAVE R AND
31     C      I AS FINAL CHARACTERS.)
32     C      ZR,ZI          REAL(DOUBLE PRECISION) TYPE INPUT
33     C      ERFZR,ERFZI    (SAME TYPE AS Z)           OUTPUT
34     C      ERFCZR,ERFCZI   "                  OUTPUT
35     C      EZ2CZR,EZ2CZI   "                  OUTPUT
36     C      IERR          INTEGER TYPE            OUTPUT
37     C      IERR          NORMAL RETURN
38     C      0              INVALID
39     C      1 EXP(Z**2)*ERFC(Z)           INVALID
40     C      2 ERF(Z),ERFC(Z)           INVALID
41     C      3 ERF(Z),ERFC(Z),EXP(Z**2)*ERFC(Z) INVALID
42     C      (Z IN 2ND OR 3RD QUADRANTS(ZR .LT. 0))
43     C      COMMONLY USED INTERNAL VARIABLES
44     C      AELL          LOWER LIMIT OF |Z| FOR ASYMPTOTIC
45     C                      EXPANSION(A.E.) ABS(ZR) .LE. 1
46     C      AZI           ABS(ZI)
47     C      AZR           ABS(ZR)
48     C      CMAX          MAXIMUM MACHINE VALUE
49     C      CMIN          MINIMUM MACHINE VALUE
50     C      REM2          MODULUS SQUARED OF RELATIVE
51     C                      ERROR(R.E.)
52     C      1R.E!**2=REM2(N)
53     C      REPN2          REM2(N-1)
54     C      RHO           ZI=SQRT(ZR**2+ZI**2)
55     C      RHCLC          LOWER LIMIT OF RHC FOR USING ONLY
56     C                      1ST TERM OF A.E.
57     C      RHOLS          UPPER LIMIT OF RHO, UNRESTRICTED

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58      C           ABS(ZR), FOR POWER SERIES
59      C           RTPI      SQRT(PI=3.14...)
60      C           SUMM2    ISUMI**2=SUMR**2+SUMI**2
61      C           OR ISUM/TMAX1**2
62      C           TMAX      NORMALIZATION FACTOR
63      C           TMM2     ITMI**2=TMR**2+TMI**2
64      C           OR ITM/TMAX1**2
65      C           TOLER     UPPER LIMIT FOR RELATIVE ERRORS
66      C           TCLER2   TCLER**2
67      C           TOL2     TCLER2/8
68      C           ULSC     MAXIMUM ARGUMENT FOR SIN/COS ROUTINE
69      C MODIFICATIONS.
70      C THE CODE IS SET UP FOR SINGLE PRECISION COMPUTATION
71      C WITH SINGLE PRECISION FUNCTION REFERENCES AND SINGLE
72      C PRECISION MACHINE DEPENDENT CONSTANTS. FOR THE UNIVAC
73      C 1108, CMAX APPFCX. 2**127, CMIN=2**(-129),ULSC=2**20 AND
74      C TOLER=.745E-8, RTPI IS GIVEN IN DOUBLE
75      C PRECISION FORMAT TO 19 SIGNIFICANT FIGURES.
76      C DOUBLE PRECISION RESULTS ARE OBTAINED BY INSERTING
77      C (1) THE DOUBLE PRECISION TYPE STATEMENT
78      C (2) DOUBLE PRECISION INTRINSIC FUNCTION REFERENCES -
79      C       DABS,CMAX1 AND CMIN1
80      C (3) DOUBLE PRECISION EXTERNAL FUNCTION REFERENCES -
81      C       DCCS,DEXP,DLOG,DSIN AND DSQRT AND
82      C (4) FOR THE UNIVAC 1108 ADJUSTING THE CONSTANTS
83      C       CMAX APPROX. 2**1023,CMIN=2**(-1025),ULSC=2**56 AND
84      C       TCLER=.E7C-18.
85      C THE DETAILED METHODS SHOULD WORK FOR ANY PRECISION
86      C IF THE MACHINE DEPENDENT CONSTANTS ARE CHANGED
87      C WITH RTPI GIVEN TO THE REQUIRED NUMBER OF SIGNIFICANT
88      C FIGURES.
89      C METHOD. Z=ZR+I ZI =RHC*EXP(I*ARCTAN(ZI/ZR))
90      C ALL METHODS APPLY TO AZ=ABS(ZR)+I ABS(ZI)=AZR+
91      C I AZI. USE IS THEN MADE OF SYMMETRY RELATIONS.
92      C POWER SERIES
93      C       RHC .LT. RHOLS(=1.5)
94      C       AZR .LE. 1, RHOLS .LE. RHO .LT. AELL
95      C               AELL=SQRT(-LOG(TOLER))
96      C       ERF(AZ)=(2/SQRT(PI))*SUM(SGN(RN)*TM(RN))
97      C               RN=0.1,...,RNF
98      C       SGN(0)=1
99      C       SGN(RN+1)=-SGN(RN)
100     C       TM(RN)=((AZ**2*(2*RN+1))/1*2...RN)/(2*RN+1)
101     C       TM(RN)=PTM(RN)/DN(RN)
102     C       PTM(0)=AZ
103     C       PTM(RN+1)=(AZ**2)*PTM(RN)/(RN+1)
104     C       DN(0)=1
105     C       DN(RN+1)=DN(RN)+2
106     C       RNF=RN IF TM=0 AND SUM=0, IF ITM/TMAX1**2(=TMM2)
107     C       =0 OR IF ISUM/TMAX1**2(=SUMM2) .NE. 0 AND
108     C       FEM2(=TMM2/SUMM2) .LT. TOLER2
109     C CONTINUED FRACTION
110     C       AZR .GT. 1, RHOLS .LE. RHO .LT. RHO1C
111     C               RHO1C=SQRT(DNE/(TNC*TOLER))
112     C       EXP(AZ**2)*ERFC(AZ)=
113     C               (2*AZ/SQRT(PI))*(1 I/I (2*(AZ**2)+1)-
114     C                               1*2 I/I (2*(AZ**2)+5)-
115     C                               3*4 I/I (2*(AZ**2)+9)-...)

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116      C          =(2*AZ/RTPI)*II(AM(RN) I/I EM(RN))
117      C          RN=1,2,...,RNF
118      C          AM(1)=1
119      C          AM(RN+1)=-WM(RN+1)*(WM(RN+1)+1)
120      C          RM(1)=2*(AZ**2)+1
121      C          BM(RN+1)=EM(RN)+4
122      C          WM(1)=-1
123      C          WM(RN+1)=WM(RN)+2
124      C          =(AZ*(FM/GM))/2/RTPI
125      C          =(AZ*F(FN))/2/RTPI
126      C          FN(-1)=1
127      C          CN(-1)=0
128      C          FN(0)=0
129      C          CN(0)=1
130      C          FM(RN)=BM(RN)*FM(RN-1)+AM(RN)*FM(RN-2)
131      C          GM(RN)=BM(RN)*GM(RN-1)+AM(RN)*GM(RN-2)
132      C          FNF=RNF IF REM2(FCR R.E.=(F(RN)-F(RN-1))/F(RN))
133      C          .LT. TOL2 OR
134      C          FNF=RNF-1 IF REM2(RN) .GE. REM2(RN-1)
135      C          ASYMFTCTIC EXPANSION
136      C          AZR .LE. 1. AELL .LE. RHO .LT. RHOLOC
137      C          (FCR FCFLC .LE. RHC .LE. CMAX, TO PRESERVE
138      C          ACCURACY AN ALTERNATIVE COMPUTATION OF
139      C          THE FIRST TERM OF THE A.E. IS EMPLOYED.)
140      C          EXP(AZ**2)*ERFC(AZ)=(SUM(SGN(FN)*TM(RN)))/SORT(PI)
141      C          RN=0,1,...,RNF
142      C          SGN(0)=1
143      C          SGN(RN+1)=-SGN(RN)
144      C          TM(RN)=(1/AZ)*(1*3...*(2*RN-1))/
145      C          (2*(AZ**2)**RN
146      C          TM(C)=1/AZ
147      C          TM(RN+1)=CN(RN+1)*(TM(RN)*(1/(2*(AZ**2))))*
148      C          CN(1)=1
149      C          CN(RN+1)=DN(RN)+2
150      C          RNF=RNF IF REM2(FCR R.E.=TM/SUM) .LT. TOL2
151      C          FNF=RNF-1 IF TMW2(RN) .GE. TMW2(RN-1)
152      C          (DIVERGENCE)
153      C          RANGE.
154      C          EXP(Z**2)*ERFC(Z) IS VALID FOR ZR .GE. 0 THROUGHOUT
155      C          THE ENTIRE MACHINE RANGE. ERF(Z),ERFC(Z) AND
156      C          EXP(Z**2)*ERFC(Z) (FCR ZR .LT. 0) ARE LIMITED BY THE
157      C          RANGE AND ACCURACY OF THE SINE,COSINE AND/OR THE
158      C          EXPONENTIAL LIBRARY ROUTINES.
159      C          ACCURACY. THE MAXIMUM RELATIVE ERROR (GENERALLY IN ERFC)
160      C          EXCEPT IN THE IMMEDIATE NEIGHBORHOOD OF ZEROS,
161      C          IS 8(-6) IN THE UNIVAC 1108 FCR
162      C          SINGLE PRECISION COMPUTATION. THE REAL
163      C          AND IMAGINARY PARTS INDEPENDENTLY AS WELL
164      C          AS THEIR ZEROS ENTER INTO CONSIDERATION.
165      C          PRECISION VARIABLE - BY SETTING A PREDETERMINED VALUE OF
166      C          TOLER
167      C          MAXIMUM UNIVAC 1108 TIME/SHARING EXECUTIVE SYSTEM
168      C          TIMING.     S.P.          D.P.
169      C          (SECCNDS)    .0101        .052
170      C          STORAGE. 1171 WORDS REQUIRED BY THE UNIVAC 1108 COMPILER
171      C          (313 FORTRAN STATEMENTS, 95 VARIABLES)
172      C          * THE PFCFT VERIFIER,A.C.HALL AND B.G.RYDER
173      C          (BELL LABORATORIES,MURRAY HILL, N.J.) PROCESSED BY THE COMPUTER

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174      C SCIENCE AND STATISTICS EIGHTH ANNUAL SYMPOSIUM ON THE
175      C INTERFACE, UNIV. OF CALIF., LOS ANGELES, FEB. 13-14, 1975.
176      *****
177      SUBROUTINE ERZR(ZR,ZI,ERFZR,ERFZI,ERFCZR,ERFCZI,
178      1                           EZ2CZR,EZ2CZI,IERR)
179      C           MACHINE DEPENDENT CONSTANTS
180      CMAX=.1701411E2E39
181      CMIN=.146936794E-38
182      ULSC=.1048576E7
183      TOLER=.745E-8
184      C NOTE TOLER IS SET TO THE PRECISION OF
185      C THE UNIVAC 1108 SINGLE PRECISION ARITHMETIC.
186      RTPI=1.7724E3E50905516027D0
187      C           OTHER CONSTANTS
188      ZERC=0
189      CNE=1
190      TWC=2
191      THREE=3
192      FOUR=4
193      CNPTFV=THREE/TWC
194      C           INITIALIZATION OF ERROR INDICATORS
195      IERR=0
196      IQ=0
197      C           FUNCTION REFERENCES
198      C NOTE FUNCTION REFERENCES OCCUR IN THE REGIONS OF STATEMENT
199      C LABELS 5, 15 AND 85 AND IN STATEMENT LABELS 110, 315, 515,
200      C 517 AND 955.
201      C           SET UP FOR Z IN FIRST QUADRANT   AZ=AZR+I AZI
202      5 AZR=AES(ZR)
203      AZI=AES(ZI)
204      ARIMN=AMIN1(AZR,AZI)
205      ARIMX=AMAX1(AZR,AZI)
206      IF (ARIMX .GT. ZERC) GO TO 10
207      C           SPECIAL CASE, Z=0
208      ERFZR=ZERO
209      ERFZI=ZERO
210      ERFCCZR=CNE
211      ERFCCZI=ZERC
212      EZ2CZR=CNE
213      EZ2CZI=ZERC
214      RETURN
215      C           CONTROL VARIABLES
216      10 TOLER2=TCLER*TCLER
217      TCL2=TCLER2/FCUR/TWC
218      RHCLS=CNPTFV
219      RMNMX=AFIMN/AFIMX
220      15 CMAXLN=ALOG(CMAX)
221      CMINLN=ALOG(CMIN)
222      AELL=SGRT(-ALCG(TOLER))
223      RHCLC=SGRT(CNE/(TWC*TOLER))
224      PRHC=SGRT(RMNMX*RMNMX+CNE)
225      C           COMPUTATION OF AUXILIARY QUANTITIES
226      C           COMPUTATION OF AZ**2=Z2R+I AZ2I
227      IF (AFIMX .LT. CNE) GO TO 60
228      C           OVERFLOW CHECK ON Z2PN=-Z2R
229      TEMPB=((CNE-RMNMX)*ARIMX)*(CNE+RMNMX)
230      IF (TEMPB .LT. CMAX/ARIMX) GO TO 20
231      TEMPC=CMAX

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232      GO TO 30
233      20 TEMFC=TEMPE*AFINX
234      30 IF (AZR-ARIMX) 50,40,50
235      40 Z2RN=-TEMPC
236      GC TC 70
237      50 Z2RN=TEMPC
238      GO TO 70
239      60 Z2RN=(AZI+AZR)*(AZI-AZR)
240      GC TC 80
241      C          CVERFLOW CHECK CN AZ2I
242      70 IF (ARIMN .LT. (CMAX/TWO)/ARIMX) GO TO 80
243      AZ2I=CMAX
244      GO TO 50
245      80 AZ2I=(TWO*ARIMN)*ARIMX
246      C          PRELIMINARY COMPUTATIONS FOR EXP(AZ**2) AND
247      C          EXP(-AZ**2)
248      C          CHECK IF VALID ARGUMENT FOR SIN/COS
249      IF (AZ2I .GE. ULSC) GO TO 90
250      85 COAZ2I=CCS(AZ2I)
251      SIAZ2I=SIN(AZ2I)
252      C          EXTENDING RANGE OF EXP RUTINE
253      90 TEMP=Z2RN/THREE
254      Z2R=-Z2RN
255
256      C          CVERFLOW CHECK
257      IF (TEMP .LT. CMAXLN) GO TO 100
258      EMZ2D3=CMAX
259      EZ2R=ZERC
260      GC TO 190
261
262      C          UNDERFLOW CHECK
263      100 IF (TEMP .GT. CMINLN) GO TO 110
264      EMZ2D3=ZERC
265      C          EXP(AZ**2) OVERFLOWS (IQ=1)
266      IQ=1
267      GC TO 160
268      110 EMZ2D6=EXP(TEMP/TWO)
269      EMZ2D3=EMZ2D6*EMZ2D6
270      EZ2D6=CNE/EMZ2D6
271      IF (EZ2D6 .LE. CNE) GO TO 180
272      J=1
273      PEXP=ZERG
274      TEMP=EZ2D6
275      120 IF (TEMP .GE. CMAX/EZ2D6) GO TO 150
276      TEMP=TEMP*EZ2D6
277      J=J+1
278      IF (J-S) 120,130,140
279      130 PEXP=TEMP
280      GO TO 120
281      140 EZ2R=TEMP
282      GO TO 190
283      150 IF (PEXP) 170,160,170
284      160 PEXP=CMAX
285      170 EZ2R=CMAX
286      GO TO 190
287      180 PEXP=EZ2D6**
288      EZ2R=PEXP*EZ2D6
289      TEZ2=(PEXP*TWC)*EZ2D6
290
291      C          CCOMPUTATION OF RHO
292      C          CVERFLOW CHECK

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290      190 IF (ARIMX .LT. CMAX/PRHO) GO TO 200
291      RHC=CMAX
292      GC TC 210
293      200 RHC=ARIMX*PRHC
294      C           METHOD SELECTION
295      210 IF (RHC .LT. RHCLC) GO TO 220
296      C           IMPRECVE ACCURACY FOR LARGE RHO
297      FA=AZR/ARIMX
298      FB=AZI/ARIMX
299      FC=RTFI*(RMNMX*RMNMX+ONE)
300      EZ2CZR=(FA/ARIMX)/FC
301      EZ2CZI=-(FB/ARIMX)/FC
302      GO TO 800
303      220 IF (RHC .LT. RHCLS) GO TO 300
304      IF (AZR .GT. CNE) GC TO 500
305      IF (RHC-AELL) 300,700,700
306      C           PCWER SERIES FOR ERF(AZ)
307      C           INITIALIZATION
308      300 SUMR=ZERG
309      SUMI=ZERG
310      SGN=CNE
311      RN=ZERC
312      DN=CNE
313      PTMR=AZR
314      PTMI=AZI
315      C           CCOMPUTING SUM
316      310 TMR=PTMR/DN
317      TMI=PTMI/DN
318      SUMR=SUMR+TMR*SGN
319      SUMI=SUMI+TMI*SGN
320      C           SCALING TO AVOID OVERFLOW OR UNDER-
321      C           FLCW IN APPROXIMATING R.E.
322      315 TMAX=AMAX1(AES(TMR),AES(TMI),ABS(SUMR),ABS(SUMI))
323      IF (TMAX) 320,360,320
324      320 TMM2=(TMR/TMAX)**2+(TMI/TMAX)**2
325      SUMM2=(SUMR/TMAX)**2+(SUMI/TMAX)**2
326      IF (TMM2) 330,360,330
327      330 IF (SUMM2) 340,350,340
328      340 REM2=TMM2/SUMM2
329      C           TOLERANCE CHECK
330      IF (REM2 .LT. TOLER2) GC TO 360
331      C           ADDITIONAL TERMS
332      350 DN=DN+TWC
333      RN=RN+CNE
334      SGN=-SGN
335      TEMF=(PTMR*Z2R-PTMI*AZ2I)/RN
336      PTMI=(PTMR*AZ2I+PTMI*Z2R)/RN
337      PTMR=TEMP
338      GC TC 310
339      C           FUNCTIONS EVALUATED IN FIRST QUADRANT
340      360 ERFZR=SUMR*TWC/RTPI
341      ERFZI=SUMI*TWC/RTPI
342      ERFCZR=CNE-ERFZR
343      ERFCZI=-ERFZI
344      EZ2CZR=(CCAZ2I*ERFCZR-SIAZ2I*ERFCZI)*EZ2R
345      EZ2CZI=(SIAZ2I*ERFCZR+CUAZ2I*ERFCZI)*EZ2R
346      GC TC 540
347      C           CCNTINUED FRACTION FOR EXP(AZ**2)*ERFC(AZ)

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343      C           INITIALIZATION
344
345      500  WM=-CNE
346          BMP=TWC*Z2E+CNE
347          BMI=TWC*AZ2I
348          AM=CNE
349          FMM2R=CNE
350          FMM2I=ZERO
351          GMM2R=ZERO
352          GMM2I=ZERO
353          FMM1R=ZERO
354          FMM1I=ZERO
355          GMM1R=CNE
356          GMM1I=ZERO
357          REFM2=CMAX
358          FPR=ZEFC
359          FPI=ZERO
360
361      C           RECURRENCE RELATION
362
363      510  FNR=EMR*FMM1R-BMI*FMM1I+AM*FMM2R
364          FMI=ENI*FMM1R+BMR*FMM1I+AM*FMM2I
365          GNR=ENR*GMM1R-BMI*GMM1I+AM*GMM2R
366          GNI=ENI*GMM1R+EMR*GMM1I+AM*GMM2I
367
368      C           CONVERGENT F=FM/GM
369
370      C           SCALING TO AVOID OVERFLOW IN
371          C COMPUTING CONVERGENT
372      515  TMAX=AMAX1(AES(FMR),ABS(FMI),ABS(GMR),ABS(GNI))
373          SFMR=FMR/TMAX
374          SFMI=FMI/TMAX
375          SGMR=GMR/TMAX
376          SGNI=GNI/TMAX
377          TEMP=SGMR*SGMR+SGNI*SGNI
378          FR=(SFMR*SGMR+SFMI*SGNI)/TEMP
379          FI=(SFMI*SGMR-SFMR*SGNI)/TEMP
380
381      C           APPROXIMATING R.E.
382          TEMP=FR*FR+FI*FI
383          TEMPA=FR-FPR
384          TEMPE=FI-FFI
385          REM2=(TEMPA*TEMPE+TEMPB*TEMPB)/TEMP
386
387      C           TOLERANCE CHECK
388          IF (REM2 .LT. TCL2) GO TO 530
389          IF (REM2 .GE. REPM2) GO TO 520
390
391      C           ADDITIONAL CONVERGENTS
392
393          WM=WM+TWC
394          EMR=EMR+FCUR
395          AM=-WM*(WM+CNE)
396          FMM2R=FMM1R
397          FMM2I=FMM1I
398          GMM2R=GMM1R
399          GMM2I=GMM1I
400          FMM1R=FMR
401          FMM1I=FMI
402          GMM1R=GMR
403          GMM1I=GNI
404          FPR=FR
405          FPI=FI
406          REFM2=REM2
407
408      C           SCALING
409      C SCALING SHOULD NOT BE DELETED AS THE VALUES OF FMR,FMI
410      C GMR,GNI MAY OVERFLOW FOR SMALL VALUES OF REAL OF Z

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406      S17    ABM=AVMAX(AES(BMR),ABS(BMI))
407      IF (TMAX .LT. (CMAX/FCUR)/(TWC*ABM-AM)) GO TO 510
408      FMM2R=FMM2R/TMAX
409      FMM2I=FMM2I/TMAX
410      GMN2R=GMN2R/TMAX
411      GMN2I=GMN2I/TMAX
412      FMM1R=FMM1R/TMAX
413      FMM1I=FMM1I/TMAX
414      GMN1R=GMN1R/TMAX
415      GMN1I=GMN1I/TMAX
416      GC TC S10
417      C           RELATIVE ERROR INCREASED-ROUNDOFFS
418      C           ACCEPT PRIOR CONVERGENT
419      S20  FR=FPR
420      FI=FPI
421      C           EVALUATE EXP(AZ**2)*ERFC(AZ)
422      S20  EZ2CZR=(AZR*FR-AZI*FI)*TWC/RTPI
423      EZ2CZI=(AZI*FR+AZR*FI)*TWC/RTPI
424      GC TC E20
425      C           ASYMPTOTIC EXPANSION FOR EXP(AZ**2)*ERFC(AZ)
426      C           INITIALIZATION
427      700  TZ2R=TWC*Z2R
428      TZ2I=TWC*A2I
429      TEMP=TZ2R*TZ2R+TZ2I*TZ2I
430      RTZ2R=TZ2R/TEMP
431      RTZ2I=-TZ2I/TEMP
432      TMW1R=(AZR/RHC)/RHC
433      TMW1I=-(AZI/RHC)/RHC
434      TMW2=TMW1R*TMW1R+TMW1I*TMW1I
435      SUMR=TMW1R
436      SUMI=TMW1I
437      DN=CNE
438      SGN=-CNE
439      C           COMPUTING SUM
440      710  TMR=CN*(TMW1R*RTZ2R-TMW1I*RTZ2I)
441      TMI=CN*(TMW1I*RTZ2R+TMW1R*RTZ2I)
442      SUMR=SGN*TMR+SUMR
443      SUMI=SGN*TMI+SUMI
444      C           APPROXIMATING R.E.
445      SUMW2=SUMR+SUMI+SUMI*SUMI
446      TMW2=TMR+TMR+TMI+TMI
447      REM2=TMW2/SUMW2
448      C           TOLERANCE CHECK
449      IF (REM2 .LT. TCL2) GO TO 730
450      IF (TMW2 .LT. TMW2) GO TO 720
451      C           DIVERGENT PATH
452      SUMR=SUMR-SGN*TMR+SGN*TMW1R
453      SUMI=SUMI-SGN*TMI+SGN*TMW1I
454      GC TC 730
455      C           ADDITIONAL TERMS
456      720  SGN=-SGN
457      DN=DN+TWO
458      TMW1R=TMR
459      TMW1I=TMI
460      TMW2=TMW2
461      GC TC 710
462      C           EVALUATE EXP(AZ**2)*ERFC(AZ)
463      730  EZ2CZR=SUMR/RTPI

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4E4      EZ2CZI=SUMI/RTPI
4E5      C          MAINTAINING ACCURACY IN EZ2CZR
4E6      C          FOR SMALL AZR
4E7      TEMPF=EZ2CZR*TCLER
4E8      IF (TEMP .GT. EZ2R) GO TO 800
4E9      TEMPF=CIN*RHCLC
470      IF (EZ2CZR .GT. TEMP) GO TO 750
471      IF (EZ2R .GT. TEMP) GO TO 750
472      IF (AZF) 740,750,740
473      C          INDICATE RESULTING ERRORS IN ERFC
474      C          (AND ERF)(IERR=2)
475      740 IERR=2
476      750 EZ2CZR=EZ2CZR+EZ2R*COAZ2I
477      C          EVALUATE ERFC AND ERF FOR AZ IN CONTINUED
478      C          FRACTION AND ASYMPTOTIC EXPANSION REGIONS
479      800 IF (AZ2I .LT. ULSC) GO TO 830
480      C          INVALID ARGUMENT FOR SIN/COS
481      C          ERFC(AND ERF) INVALID (IERR=2)
482      IF (AZR=ARIMX) E20,810,820
483      C          AZR .GE. AZI
484      810 ERFCZR=ZERO
485      ERFCZI=ZERO
486      GC TC S10
487      C          AZR .LT. AZI
488      820 ERFCZR=CMAX
489      ERFCZI=CMAX
490      GC TC S10
491      C          VALID ARGUMENT FOR SIN/COS
492      830 IF (RFC .GE. RHOLC) GO TO 840
493      C          RFC .LT. RHOLC
494      TEMPA=EZ2CZR*CCAZ2I+EZ2CZI*SIAZ2I
495      TEMFB=-EZ2CZR*SIAZ2I+EZ2CZI*COAZ2I
496      TEMPC=EMZ2D3
497      GG TC E50
498      C          RFC .GE. RHOLC
499      E40 TEMPA=(FA*CCAZ2I-FB*SIAZ2I)/FC
500      TEMPB=(-FA*SIAZ2I-FB*COAZ2I)/FC
501      TEMPF=EMZ2D2/AFIMX
502      TEMPA=TEMPA*TEMF
503      TEMFB=TEMPB*TEMF
504      TEMFC=CNE
505      E50 IF (EMZ2D3 .LE. CNE) GO TO 920
506      C          EVALUATE ERFC(AZ)(AZI .GT. AZR)
507      I=1
508      TEMPF=TEMFA
509      E60 J=1
510      SGN=CNE
511      FD=TEMFC
512      IF (TEMP .GE. ZERO) GO TO 870
513      SGN=-SGN
514      TEMF=-TEMP
515      E70      IF (TEMP .LT. CMAX/FD) GO TO 880
516      TEMPF=CMAX
517      IC=2
518      GC TC 850
519      E80      TEMP=TEMP*FD
520      J=J+1
521      IF (J .GT. 3) GC TO 890

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522          FD=EMZ2C3
523          GC TO 870
524      890  IF ( I .GE. 2) GO TO 900
525          ERFCZR=TEMP*SGN
526          I=I+1
527          TEMP=TEMPE
528          GC TC 860
529      900  ERFCZI=TEMP*SGN
530          IF ( IC .NE. 2) GO TO 930
531      C           ERFC(AND ERF) INVALID ( IERR=2)
532      C           OVERFLW CF ERFC(AZ)( IQ=2)
533      910  IERR=2
534          GC TC 530
535      C           EVALUATE ERFC(AZ)(AZI .LE. AZR)
536      920  ERFCZR=(TEMPA*EMZ2D3)*EMZ2D3*TEMPC
537          ERFCZI=(TEMPE*EMZ2D3)*EMZ2D3*TEMPC
538      C           SPECIAL CASE (AZR=0)
539      930  IF (AZR .LE. ZERG) ERFCZR=CNE
540      C           EVALUATE ERF(AZ)
541          ERFZR=CNE-ERFCZR
542          ERFZI=-ERFCZI
543      C           SYMMETRY RELATCNNS APPLIED
544      940  IF (ZR-AZR) 950,1000,950
545      C           REAL CF Z .LT. 0
546      950  ERFZR=-ERFCZR
547          ERFCZR=TWO-ERFCZR
548          IF (AZ2I .GE. ULSC) GO TO 960
549          IF (IC .EQ. 1) GO TC 960
550      C           MAINTAINING ACCURACY IN 2*EXP(Z**2)
551          IF (AZR .LE. AZI) GO TO 980
552          S55 TEMP=A MAX1(AES(SIAZ2I), ABS(COAZ2I))
553          IF (TEMP .LT. ((CMAX/TWO)/PEXP)/EZ2D6) GO TC 570
554          C           EXP(Z**2)*ERFC(Z) INVALID (IERR+1)
555      960  IERR=IERR+1
556          EZ2CZR=CMAX
557          EZ2CZI=CMAX
558          GO TO 1000
559      970  TEZ2R=((PEXP*(CAZ2I)*EZ2D6)*TWO
560          TEZ2I=((PEXP*SIAZ2I)*EZ2D6)*TWC
561          GC TO 590
562      980  TEZ2R=TEZ2*CCAZ2I
563          TEZ2I=TEZ2*SIAZ2I
564      C           EVALUATE EXP(Z**2)*ERFC(Z)
565      990  EZ2CZR=TEZ2R-EZ2CZR
566          EZ2CZI=EZ2CZI-TEZ2I
567      1000  IF (ZI-AZI) 1010,1020,1010
568      C           IMAGINAFY OF Z .LT. 0
569      1010  ERFZI=-ERFZI
570          ERFCZI=-ERFCZI
571          EZ2CZI=-EZ2CZI
572      1020  RETURN
573          END

```

TABLE 1

ERFC(Z)

RHO\THETA	0°	15°	30°	37.5°	45°
.00	.100000+01 .0	.100000+01 .000000	.100000+01 .000000	.100000+01 .000000	.100000+01 .000000
.02	.977435+00 .0	.978204+00 -.583879-02	.980456+00 -.112808-01	.982095+00 -.137355-01	.984040+00 -.159556-01
.04	.954889+00 .0	.956420+00 -.116648-01	.960912+00 -.225435-01	.964183+00 -.274543-01	.968068+00 -.318984-01
.06	.932378+00 .0	.934662+00 -.174654-01	.941368+00 -.337702-01	.946257+00 -.411398-01	.952070+00 -.478156-01
.08	.909922+00 .0	.912942+00 -.232279-01	.921824+00 -.449428-01	.928310+00 -.547751-01	.936033+00 -.636943-01
.10	.887537+00 .0	.891273+00 -.289397-01	.902280+00 -.560434-01	.910337+00 -.683437-01	.919946+00 -.795217-01
.12	.865242+00 .0	.869667+00 -.345886-01	.882738+00 -.670542-01	.892330+00 -.818288-01	.903796+00 -.952846-01
.14	.843053+00 .0	.848138+00 -.401625-01	.863197+00 -.779575-01	.874283+00 -.952136-01	.887571+00 -.110970+00
.16	.820988+00 .0	.826697+00 -.456493-01	.843657+00 -.887357-01	.856190+00 -.108481+00	.871258+00 -.126564+00
.18	.799064+00 .0	.805358+00 -.510376-01	.824121+00 -.993713-01	.838045+00 -.121615+00	.854845+00 -.142053+00
.20	.777297+00 .0	.784132+00 -.563161-01	.804590+00 -.109847+00	.819844+00 -.134598+00	.838321+00 -.157424+00
.30	.671373+00 .0	.680129+00 -.806921-01	.707071+00 -.159241+00	.727824+00 -.196662+00	.753652+00 -.231995+00
.40	.571608+00 .0	.580740+00 -.100871+00	.610081+00 -.202202+00	.633845+00 -.252418+00	.664672+00 -.301347+00
.50	.479500+00 .0	.487320+00 -.115988+00	.514270+00 -.236937+00	.537866+00 -.299764+00	.570447+00 -.363359+00
.60	.396144+00 .0	.401058+00 -.125565+00	.420627+00 -.261983+00	.440342+00 -.336667+00	.470518+00 -.415645+00
.70	.322199+00 .0	.322926+00 -.129533+00	.330478+00 -.276308+00	.342317+00 -.361274+00	.365070+00 -.455585+00
.80	.257899+00 .0	.253631+00 -.128213+00	.245436+00 -.279418+00	.245465+00 -.372052+00	.255106+00 -.480414+00
.90	.203092+00 .0	.193577+00 -.122258+00	.167296+00 -.271437+00	.152078+00 -.367979+00	.142621+00 -.487404+00
1.00	.157299+00 .0	.142847+00 -.112577+00	.978859-01 -.253165+00	.649787-01 -.348749+00	.307358-01 -.474148+00
1.10	.119795+00 .0	.101201+00 -.100228+00	.388720-01 -.226077+00	.126659-01 -.314972+00	.762502-01 -.438939+00
1.20	.896860-01 .0	.680972-01 -.863111-01	.844458-02 -.192259+00	.776217-01 -.268341+00	.172938+00 -.381252+00
1.30	.659921-01 .0	.427427-01 -.718743-01	.433244-01 -.154271+00	.126958+00 -.211694+00	.253111+00 -.302268+00
1.40	.477149-01 .0	.241557-01 -.578252-01	.657413-01 -.114934+00	.158478+00 -.148963+00	.310259+00 -.205369+00
1.50	.338949-01 .0	.112438-01 -.448760-01	.764609-01 -.770708-01	.171150+00 -.849352-01	.338390+00 -.965018-01
1.60	.236516-01 .0	.288326-02 -.335145-01	.577020-02 -.432136-01	.165457+00 -.248347-01	.333094+00 -.157600-01
1.70	.162095-01 .0	.-200643-02 -.240031-01	.696000-01 -.153368-01	.143694+00 .262601-01	.292775+00 .120601+00
1.80	.109095-01 .0	.-440212-02 -.164025-01	.567976-01 .535338-02	.109748+00 .641075-01	.219843+00 .205946+00
1.90	.720957-02 .0	.-513475-02 -.106123-01	.413301-01 .185261-01	.689521-01 .859866-01	.121580+00 .260096+00
2.00	.467773-02 .0	.-486777-02 -.641967-02	.257133-01 .247077-01	.273484-01 .912368-01	.103117-01 .273926+00
2.10	.297947-02 .0	.-409504-02 -.354979-02	.119733-01 .251347-01	.916428-02 .815039-01	.974865-01 .243355+00
2.20	.186285-02 .0	.-315468-02 -.170957-02	.144281-02 .215037-01	.358034-01 .605788-01	.183390+00 .171536+00
2.30	.114318-02 .0	.-225377-02 -.621965-03	.531949-02 .156622-01	.497620-01 .337876-01	.230486+00 .700421-01
2.40	.688514-03 .0	.-149843-02 -.481389-04	.847425-02 .930477-02	.507367-01 .700451-02	.227631+00 -.417236-01
2.50	.406952-03 .0	.-924217-03 .201683-03	.872881-02 .372996-02	.409438-01 -.145264-01	.173531+00 -.139462+00
2.60	.236034-03 .0	.-523179-03 .266848-03	.709056-02 -.293708-03	.245557-01 -.272819-01	.792740-01 -.199249+00
2.70	.134333-03 .0	.-265334-03 .241454-03	.460569-02 -.253794-02	.664754-02 -.301636-01	.321336-01 -.204295+00
2.80	.750132-04 .0	.-113783-03 .181327-03	.214179-02 -.321372-02	.809354-02 -.245881-01	.130194+00 -.151392+00
2.90	.410979-04 .0	.-339435-04 .122861-03	.256793-03 -.279917-02	.165397-01 -.138997-01	.185124+00 -.545715-01
3.00	.220905-04 .0	.198248-05 .741051-04	.830403-03 -.184961-02	.178141-01 -.225516-02	.178018+00 .564096-01
3.50	.743098-06 .0	.383634-05 -.331302-06	.361438-04 .343118-03	.663124-02 .774278-03	.146013+00 -.667835-01
4.00	.154173-07 .0	.-506480-07 -.121829-06	.-100583-04 -.454411-04	.-206887-02 .808579-03	.-704373-01 .121816+00
4.50	.196616-09 .0	.-172664-08 .241877-08	.342245-05 .358814-05	.149447-03 -.641621-03	.-697054-01 -.103987+00
5.00	.153746-11 .0	.-431344-10 -.812606-11	.-410390-06 .690194-07	.163226-03 .593711-04	.909031-01 -.666628-01
5.50	.735785-14 .0	.-401550-12 -.137042-12	.-98839-10 -.274562-07	.529439-06 .406179-04	.945377-01 .396363-01
6.00	.215197-16 .0	.-222076-14 .150084-14	.136924-08 -.383336-09	.-550781-05 .636094-05	.563713-01 .752047-01
6.50	.384215-19 .0	.-905982-17 -.633184-17	.477805-10 .324007-10	.-126107-05 .886874-06	.498547-01 .710156-01
7.00	.418383-22 .0	.-276523-19 .109112-19	.941894-12 .157585-11	.-164519-06 .187753-06	.710858-01 .379415-01
7.50	.277665-25 .0	.-517996-22 .562585-23	.233092-13 .393021-13	.525818-10 .356932-07	.667858-01 .345871-01
8.00	.112243-28 .0	.-396093-25 -.443759-25	.731135-15 .506747-15	.420606-08 .160997-08	.-258232-01 .656143-01
8.50	.276232-32 .0	.-111560-28 .427748-28	.130972-16 -.343079-17	.123912-09 -.485650-09	.-475602-01 .462887-01
9.00	.413703-36 .0	.-213063-31 -.174915-32	.313042-20 -.160996-18	.-462157-10 .168052-10	.623821-01 -.612171-02

## ERFC(Z)

RHONTHETA	50°	60°	70°	80°	90°	
.00	.100000+01	.000000	.100000+01	.000000	.100000+01	.000000
.02	.985491+00	-.172863-01	.988713+00	-.195441-01	.992279+00	-.212081-01
.04	.970967+00	-.345635-01	.977408+00	-.390882-01	.984542+00	-.424252-01
.06	.956411+00	-.518226-01	.966067+00	-.586322-01	.976774+00	-.636604-01
.08	.941809+00	-.690545-01	.954672+00	-.781761-01	.968559+00	-.849226-01
.10	.927144+00	-.862497-01	.943204+00	-.977195-01	.961080+00	-.106221+00
.12	.912401+00	-.103399+00	.931646+00	-.117262+00	.953123+00	-.127564+00
.14	.897565+00	-.120493+00	.919978+00	-.136803+00	.945070+00	-.148961+00
.16	.882621+00	-.137521+00	.908183+00	-.156342+00	.936906+00	-.170421+00
.18	.867552+00	-.154473+00	.896242+00	-.175878+00	.928612+00	-.191952+00
.20	.852345+00	-.171339+00	.884135+00	-.155409+00	.920173+00	-.213564+00
.30	.773712+00	-.253982+00	.820454+00	-.292919+00	.875153+00	-.323124+00
.40	.689468+00	-.332643+00	.749698+00	-.389843+00	.823615+00	-.435932+00
.50	.558041+00	-.405420+00	.669242+00	-.485367+00	.762712+00	-.552889+00
.60	.498195+00	-.469950+00	.576286+00	-.578076+00	.688562+00	-.674665+00
.70	.389205+00	-.523342+00	.467898+00	-.665719+00	.598036+00	-.801524+00
.80	.271098+00	-.562163+00	.341135+00	-.744933+00	.484501+00	-.933057+00
.90	.144933+00	-.582512+00	.193283+00	-.810912+00	.341532+00	-.106775+01
1.00	.131385-01	-.580211+00	.222736-01	-.857061+00	.160625+00	-.120233+01
1.10	-.120165+00	-.551166+00	.172655+00	-.874670+00	.686592-01	-.133079+01
1.20	-.248882+00	-.491928+00	.389989+00	-.852699+00	.358812+00	-.144298+01
1.30	-.364829+00	-.400481+00	.624572+00	-.777828+00	.724161+00	-.152248+01
1.40	-.457890+00	-.277246+00	.865837+00	-.635009+00	.118000+01	-.154380+01
1.50	-.516623+00	-.126215+00	.109565+01	-.408856+00	.174051+01	-.146840+01
1.60	-.529455+00	.439353-01	.128600+01	-.863300-01	.241452+01	-.123975+01
1.70	-.486589+00	.219059+00	.139708+01	.338770+00	.319777+01	-.777391+00
1.80	-.382619+00	.379468+00	.137659+01	.859011+00	.405945+01	.291660-01
1.90	-.219614+00	.501081+00	.116196+01	.144402+01	.452009+01	.132454+01
2.00	-.101646-01	.558267+00	.687539+00	.202914+01	.561710+01	.328529+01
2.10	.220530+00	.528666+00	.100155+00	.250402+01	.585370+01	.610278+01
2.20	.434783+00	.399806+00	.121649+01	.270506+C1	.512891+01	.993582+01
2.30	.586112+00	.176582+00	.260024+01	.241951+01	.265168+01	.148074+02
2.40	.627560+00	-.112358+00	.406480+01	.141207+01	.274334+01	.204062+02
2.50	.524677+00	-.412231+00	.524907+01	-.511462+00	.126293+02	.257378+02
2.60	.271303+00	-.647141+00	.559076+01	-.339050+01	.288616+02	.285642+02
2.70	-.961516-01	-.735157+00	.436233+01	-.694257+01	.530807+02	.245883+02
2.80	-.492661+00	-.613886+00	.827238+00	-.103663+02	.854677+02	.644245+01
2.90	-.794447+00	-.271241+00	.542122+01	-.121876+02	.122167+03	-.371981+02
3.00	-.870118+00	.227570+00	-.139065+02	-.102944+02	.150602+03	-.121463+03
3.50	.128375+01	-.438817+00	.436770+02	.609546+C2	-.181518+04	-.696951+03
4.00	-.143233+01	.176970+01	.286672+03	-.315634+03	.142504+05	.268505+05
4.50	-.153046+01	.394580+01	.303475+04	.899044+03	-.581405+05	-.694896+06
5.00	.818979+01	-.289861+01	.236016+05	.194203+05	-.301677+05	.237891+08
5.50	.141149+02	.136673+02	.192298+06	-.331209+06	-.279467+09	-.117057+10
6.00	.892289+01	.480481+02	.434927+07	-.444020+07	.640472+11	.633707+11
6.50	.767743+01	.133290+03	.130111+09	.950077+07	-.952019+13	.967322+12
7.00	.164446+03	.364872+03	.308919+10	.172358+10	.442269+15	-.156615+16
7.50	.126058+04	.375323+03	.107926+12	.606848+11	.371118+18	.125665+18
8.00	.231199+04	-.413300+04	.557097+13	.462008+12	-.785527+19	.138783+21
8.50	-.181429+05	-.441024+04	.231401+15	-.228725+15	-.624892+23	.370071+23
9.00	.404091+05	.697050+05	-.117844+17	-.213680+17	-.554262+26	-.688648+25

TABLE 2

EXP{Z\*\*2}\*ERFC(Z)

RHO\THETA	0°	15°	30°	37.5°	45°
.00	.100000+01 .0	.100000+01 .000000	.100000+01 .000000	.100000+01 .000000	.100000+01 .000000
.02	.977826+00 .0	.978544+00 -.564511-02	.980656+00 -.109433-01	.982202+00 -.133574-01	.984046+00 -.155619-01
.04	.956418+00 .0	.957755+00 -.109148-01	.961711+00 -.212290-01	.964623+00 -.259749-01	.968117+00 -.303494-01
.06	.935741+00 .0	.937610+00 -.158323-01	.943165+00 -.308907-01	.947276+00 -.378843-01	.952236+00 -.443878-01
.08	.915764+00 .0	.918086+00 -.204192-01	.925014+00 -.399605-01	.930171+00 -.491167-01	.936422+00 -.577025-01
.10	.896457+00 .0	.899159+00 -.246960-01	.907257+00 -.484692-01	.913315+00 -.597018-01	.920696+00 -.703184-01
.12	.877791+00 .0	.880810+00 -.286817-01	.889890+00 -.564458-01	.896717+00 -.696688-01	.905075+00 -.822605-01
.14	.859740+00 .0	.863016+00 -.323942-01	.872908+00 -.639183-01	.880383+00 -.790455-01	.889575+00 -.935532-01
.16	.842277+00 .0	.845758+00 -.358502-01	.856308+00 -.709132-01	.864318+00 -.878590-01	.874212+00 -.104221+00
.18	.825378+00 .0	.829017+00 -.390656-01	.840085+00 -.774557-01	.848526+00 -.961353-01	.858998+00 -.114286+00
.20	.809020+00 .0	.812775+00 -.420551-01	.824233+00 -.835698-01	.833010+00 -.103900+00	.843946+00 -.123774+00
.30	.734559+00 .0	.738441+00 -.540691-01	.750340+00 -.108476+00	.759640+00 -.135855+00	.771453+00 -.163319+00
.40	.670788+00 .0	.674177+00 -.621855-01	.684812+00 -.125660+00	.693269+00 -.158259+00	.704192+00 -.191604+00
.50	.615690+00 .0	.618355+00 -.674592-01	.626815+00 -.137032+00	.633647+00 -.173298+00	.642609+00 -.210932+00
.60	.567805+00 .0	.569635+00 -.706620-01	.575515+00 -.144060+00	.580342+00 -.182718+00	.586778+00 -.223250+00
.70	.525930+00 .0	.526911+00 -.723596-01	.530125+00 -.147863+00	.532829+00 -.187900+00	.536524+00 -.230166+00
.80	.489101+00 .0	.489272+00 -.729681-01	.489917+00 -.149296+00	.490547+00 -.189926+00	.491521+00 -.232989+00
.90	.456532+00 .0	.455962+00 -.727939-01	.454239+00 -.149005+00	.452940+00 -.189631+00	.451358+00 -.232766+00
1.00	.427584+00 .0	.426354+00 -.720633-01	.422513+00 -.147478+00	.419480+00 -.187662+00	.415588+00 -.230320+00
1.10	.401730+00 .0	.399923+00 -.709434-01	.394231+00 -.145081+00	.389679+00 -.184510+00	.383760+00 -.226295+00
1.20	.378537+00 .0	.376233+00 -.695576-01	.368549+00 -.142090+00	.363094+00 -.180548+00	.355440+00 -.221186+00
1.30	.357643+00 .0	.354916+00 -.679971-01	.346284+00 -.138710+00	.339332+00 -.176056+00	.330223+00 -.215369+00
1.40	.338744+00 .0	.335662+00 -.663291-01	.325505+00 -.135093+00	.318044+00 -.171244+00	.307738+00 -.209128+00
1.50	.321585+00 .0	.318209+00 -.646029-01	.307525+00 -.131350+00	.298923+00 -.166267+00	.287653+00 -.202672+00
1.60	.305953+00 .0	.302334+00 -.628545-01	.290896+00 -.127564+00	.281701+00 -.161236+00	.269672+00 -.196156+00
1.70	.291663+00 .0	.287848+00 -.611100-01	.275808+00 -.123794+00	.266147+00 -.156235+00	.253535+00 -.189690+00
1.80	.278560+00 .0	.274589+00 -.553879-01	.262075+00 -.120081+00	.252058+00 -.151319+00	.239013+00 -.183351+00
1.90	.266509+00 .0	.262415+00 -.577015-01	.249540+00 -.116455+00	.239260+00 -.146528+00	.225508+00 -.177191+00
2.00	.255396+00 .0	.251208+00 -.560596-01	.238065+00 -.112935+00	.227600+00 -.141889+00	.214048+00 -.171246+00
2.10	.245119+00 .0	.240863+00 -.544681-01	.227532+00 -.109534+00	.216948+00 -.137417+00	.203282+00 -.165535+00
2.20	.235593+00 .0	.231289+00 -.529306-01	.217837+00 -.106258+00	.207188+00 -.133122+00	.193480+00 -.160688+00
2.30	.226742+00 .0	.222408+00 -.514490-01	.208891+00 -.103112+00	.198222+00 -.129008+00	.184530+00 -.154849+00
2.40	.218499+00 .0	.214150+00 -.500239-01	.200615+00 -.100095+00	.189963+00 -.125073+00	.176334+00 -.149876+00
2.50	.210806+00 .0	.206456+00 -.486549-01	.192941+00 -.972068-01	.182336+00 -.121315+00	.168808+00 -.145143+00
2.60	.203613+00 .0	.199271+00 -.473413-01	.185809+00 -.944437-01	.175275+00 -.117730+00	.161878+00 -.140642+00
2.70	.196874+00 .0	.192549+00 -.460815-01	.179166+00 -.918020-01	.168723+00 -.114311+00	.155479+00 -.136364+00
2.80	.190549+00 .0	.186248+00 -.448740-01	.172967+00 -.892774-01	.162630+00 -.111051+00	.149556+00 -.132298+00
2.90	.184602+00 .0	.180331+00 -.437168-01	.167168+00 -.868650-01	.156950+00 -.107943+00	.144061+00 -.128434+00
3.00	.179001+00 .0	.174766+00 -.426079-01	.161735+00 -.845599-01	.151645+00 -.104980+00	.138950+00 -.124761+00
3.50	.155294+00 .0	.151281+00 -.377161-01	.139036+00 -.744669-01	.129658+00 -.920841-01	.117989+00 -.108897+00
4.00	.136999+00 .0	.133241+00 -.337346-01	.121846+00 -.663430-01	.113196+00 -.817946-01	.102526+00 -.963790-01
4.50	.122485+00 .0	.118978+00 -.304579-01	.108404+00 -.597166-01	.100432+00 -.734593-01	.906646-01 -.863253-01
5.00	.110705+00 .0	.107435+00 -.277278-01	.976147-01 -.542350-01	.902530-01 -.666012-01	.812804-01 -.781076-01
5.50	.100962+00 .0	.979088-01 -.254257-01	.887699-01 -.496392-01	.819492-01 -.608785-01	.736702-01 -.712820-01
6.00	.927766-01 .0	.899189-01 -.234628-01	.813899-01 -.457386-01	.750469-01 -.560327-01	.673730-01 -.655313-01
6.50	.858057-01 .0	.831244-01 -.217720-01	.751399-01 -.423911-01	.692192-01 -.518878-01	.620749-01 -.606252-01
7.00	.798001-01 .0	.772774-01 -.203020-01	.697797-01 -.394900-01	.642331-01 -.483034-01	.575547-01 -.563934-01
7.50	.745737-01 .0	.721940-01 -.190134-01	.651322-01 -.369532-01	.599186-01 -.451749-01	.536520-01 -.527075-01
8.00	.669852-01 .0	.677345-01 -.178753-01	.610646-01 -.347176-01	.561483-01 -.424219-01	.502479-01 -.494694-01
8.50	.659251-01 .0	.637913-01 -.168633-01	.574747-01 -.327332-01	.528254-01 -.399814-01	.472522-01 -.466031-01
9.00	.623077-01 .0	.602800-01 -.159579-01	.542832-01 -.309606-01	.498745-01 -.378036-01	.445953-01 -.440484-01

## EXP(Z\*\*2)\*ERFC(Z)

RHONTHETA	50°	60°	70°	80°	90°
.00	.100000+01 .000000	.100000+01 .000000	.100000+01 .000000	.100000+01 .000000	.100000+01 .000000
.02	.985430+00 -.168969-01	.988522+00 -.191978-01	.991980+00 -.209465-01	.995708+00 -.220828-01	.999600+00 -.225616-01
.04	.970750+00 -.330243-01	.976680+00 -.377036-01	.983379+00 -.413619-01	.990684+00 -.438614-01	.998401+00 -.450871-01
.06	.955991+00 -.484013-01	.964508+00 -.555200-01	.974228+00 -.612308-01	.984947+00 -.653065-01	.996406+00 -.675405-01
.08	.941179+00 -.630470-01	.952039+00 -.726507-01	.964559+00 -.805399-01	.978518+00 -.863902-01	.993620+00 -.898862-01
.10	.926338+00 -.769813-01	.939307+00 -.891010-01	.954404+00 -.992775-01	.971421+00 -.107086+00	.990050+00 -.112089+00
.12	.911494+00 -.902242-01	.926342+00 -.104877+00	.943794+00 -.117434+00	.963679+00 -.127369+00	.985703+00 -.134113+00
.14	.896667+00 -.102796+00	.913175+00 -.119987+00	.932761+00 -.135001+00	.955317+00 -.147215+00	.980591+00 -.155925+00
.16	.881878+00 -.114717+00	.899834+00 -.134439+00	.921336+00 -.151972+00	.946360+00 -.166602+00	.974725+00 -.177491+00
.18	.867146+00 -.126007+00	.886348+00 -.148243+00	.909551+00 -.168342+00	.936834+00 -.185511+00	.968119+00 -.198777+00
.20	.852490+00 -.136687+00	.872742+00 -.161410+00	.897434+00 -.184108+00	.926768+00 -.203921+00	.960789+00 -.219753+00
.30	.780858+00 -.181638+00	.803774+00 -.218107+00	.832921+00 -.253864+00	.869300+00 -.287964+00	.913931+00 -.318916+00
.40	.713036+00 -.214294+00	.735131+00 -.260834+00	.764351+00 -.308806+00	.802581+00 -.357672+00	.852144+00 -.406153+00
.50	.649979+00 -.236926+00	.668830+00 -.291462+00	.694712+00 -.349876+00	.730181+00 -.412479+00	.778801+00 -.478925+00
.60	.592156+00 -.251548+00	.606260+00 -.311920+00	.626410+00 -.378484+00	.655426+00 -.452678+00	.697676+00 -.535713+00
.70	.539686+00 -.259892+00	.548281+00 -.324060+00	.561255+00 -.396308+00	.581214+00 -.479263+00	.612626+00 -.576042+00
.80	.492447+00 -.263412+00	.495329+00 -.329575+00	.500496+00 -.405125+00	.509895+00 -.493727+00	.527292+00 -.600412+00
.90	.450161+00 -.263301+00	.447520+00 -.329960+00	.444890+00 -.406682+00	.443222+00 -.497872+00	.444858+00 -.610142+00
1.00	.412460+00 -.260519+00	.404741+00 -.326488+00	.394786+00 -.402602+00	.382368+00 -.493623+00	.367879+00 -.607158+00
1.10	.378934+00 -.255830+00	.366725+00 -.320215+00	.350217+00 -.394324+00	.327976+00 -.482883+00	.298197+00 -.593761+00
1.20	.349161+00 -.249826+00	.333111+00 -.311994+00	.310985+00 -.383080+00	.280243+00 -.467415+00	.236928+00 -.572397+00
1.30	.322730+00 -.242965+00	.303494+00 -.302503+00	.276740+00 -.369883+00	.239021+00 -.448772+00	.184520+00 -.545456+00
1.40	.299256+00 -.235593+00	.277452+00 -.292262+00	.247038+00 -.355543+00	.203909+00 -.428255+00	.140858+00 -.515113+00
1.50	.278384+00 -.227969+00	.254575+00 -.281666+00	.221396+00 -.340682+00	.174350+00 -.406909+00	.105399+00 -.483227+00
1.60	.259793+00 -.220280+00	.234476+00 -.271004+00	.199324+00 -.325767+00	.149701+00 -.385528+00	.773047-01 -.451284+00
1.70	.243198+00 -.212662+00	.216798+00 -.260483+00	.180352+00 -.311128+00	.129300+00 -.364688+00	.555762-01 -.420388+00
1.80	.228349+00 -.205210+00	.201224+00 -.250247+00	.164045+00 -.296992+00	.112501+00 -.344773+00	.391639-01 -.391291+00
1.90	.215025+00 -.197986+00	.187470+00 -.240389+00	.150014+00 -.283502+00	.987098-01 -.326022+00	.270518-01 -.364437+00
2.00	.203034+00 -.191033+00	.175289+00 -.230965+00	.137912+00 -.270739+00	.873971-01 -.308553+00	.183156-01 -.340026+00
2.10	.192211+00 -.184372+00	.164467+00 -.222006+00	.127441+00 -.258737+00	.781048-01 -.292400+00	.121552-01 -.318073+00
2.20	.182411+00 -.178015+00	.154819+00 -.213521+00	.118345+00 -.247499+00	.704459-01 -.277541+00	.790705-02 -.298468+00
2.30	.173510+00 -.171964+00	.146185+00 -.205507+00	.110409+00 -.237007+00	.641001-01 -.263913+00	.504176-02 -.281026+00
2.40	.165400+00 -.166214+00	.138430+00 -.197951+00	.103450+00 -.227227+00	.588065-01 -.251431+00	.315111-02 -.265522+00
2.50	.157988+00 -.160758+00	.131439+00 -.190836+00	.973162-01 -.218118+00	.543547-01 -.240002+00	.193045-02 -.251723+00
2.60	.151195+00 -.155584+00	.125111+00 -.184138+00	.918812-01 -.209636+00	.505775-01 -.229528+00	.115523-02 -.239403+00
2.70	.144950+00 -.150680+00	.119364+00 -.177833+00	.870395-01 -.201733+00	.473424-01 -.219915+00	.682328-03 -.228355+00
2.80	.139193+00 -.146031+00	.114124+00 -.171899+00	.827037-01 -.194364+00	.445450-01 -.211075+00	.393669-03 -.218399+00
2.90	.133871+00 -.141624+00	.109330+00 -.166309+00	.788013-01 -.187486+00	.421033-01 -.202926+00	.222630-03 -.209377+00
3.00	.128940+00 -.137445+00	.104930+00 -.161041+00	.752717-01 -.181058+00	.399530-01 -.195396+00	.123410-03 -.201157+00
3.50	.108892+00 -.119509+00	.874505-01 -.138780+00	.617088-01 -.154443+00	.321214-01 -.165001+00	.478512-05 -.168830+00
4.00	.942797-01 -.105481+00	.750909-01 -.121741+00	.525024-01 -.134607+00	.270928-01 -.143006+00	.112535-06 -.145954+00
4.50	.831655-01 -.942896-01	.658787-01 -.108356+00	.458048-01 -.119295+00	.235275-01 -.126308+00	.160523-08 -.128735+00
5.00	.744259-01 -.851875-01	.587346-01 -.975919-01	.406890-01 -.107125+00	.208412-01 -.113170+00	.138879-10 -.115246+00
5.50	.673700-01 -.776560-01	.530232-01 -.887858-01	.366399-01 -.972205-01	.187325-01 -.102546+00	.728772-13 -.104367+00
6.00	.615511-01 -.713293-01	.483467-01 -.813834-01	.333477-01 -.890010-01	.170271-01 -.937703-01	.231952-15 -.953962-01
6.50	.566679-01 -.659441-01	.444434-01 -.751362-01	.306137-01 -.820692-01	.156161-01 -.863935-01	.447773-18 -.878644-01
7.00	.525101-01 -.613075-01	.411335-01 -.697775-01	.283042-01 -.761436-01	.144276-01 -.801029-01	.524289-21 -.814475-01
7.50	.489261-01 -.572750-01	.382898-01 -.651309-01	.263257-01 -.710192-01	.134115-01 -.746733-01	.372336-24 -.759126-01
8.00	.458040-01 -.537368-01	.358190-01 -.610637-01	.246107-01 -.665434-01	.125322-01 -.699379-01	.160381-27 -.710891-01
8.50	.430594-01 -.506078-01	.336516-01 -.574741-01	.231091-01 -.626001-01	.117632-01 -.657709-01	.419009-31 -.668445-01
9.00	.406273-01 -.478214-01	.317343-01 -.542828-01	.217828-01 -.590993-01	.110848-01 -.620752-01	.663968-35 -.630821-01

TABLE 3

EXP(Z\*\*2)\*ERFC(-Z)

RHO\THETA	0°	15°	30°	37.5°	45°
.00	.100000+01 .0	.100000+01 .000000	.100000+01 .000000	.100000+01 .000000	.100000+01 .000000
.02	.102257+01 .0	.102215+01 .604525-02	.101974+01 .116363-01	.101801+01 .141302-01	.101595+01 .163619-01
.04	.104678+01 .0	.104502+01 .125170-01	.103989+01 .240025-01	.103620+01 .290671-01	.103188+01 .335494-01
.06	.107147+01 .0	.106863+01 .194435-01	.106043+01 .371373-01	.105458+01 .448455-01	.104775+01 .515878-01
.08	.109708+01 .0	.109302+01 .268548-01	.108137+01 .510811-01	.107311+01 .615009-01	.106354+01 .705024-01
.10	.112364+01 .0	.111821+01 .347829-01	.110269+01 .658763-01	.109177+01 .790701-01	.107920+01 .903181-01
.12	.115122+01 .0	.114424+01 .432622-01	.112441+01 .815669-01	.111056+01 .975904-01	.109472+01 .111059+00
.14	.117985+01 .0	.117112+01 .523294-01	.114650+01 .981992-01	.112943+01 .117100+00	.111004+01 .132751+00
.16	.120958+01 .0	.119891+01 .620234-01	.116896+01 .115821+00	.114836+01 .137638+00	.112513+01 .155415+00
.18	.124048+01 .0	.122763+01 .723862-01	.119178+01 .134483+00	.116733+01 .159244+00	.113995+01 .179075+00
.20	.127260+01 .0	.125731+01 .834622-01	.121495+01 .154237+00	.118629+01 .181958+00	.115445+01 .203753+00
.30	.145375+01 .0	.142149+01 .151332+00	.133536+01 .271371+00	.127976+01 .313595+00	.122045+01 .343076+00
.40	.167623+01 .0	.161572+01 .245769+00	.146100+01 .424910+00	.136645+01 .479143+00	.127026+01 .510240+00
.50	.195236+01 .0	.184573+01 .377084+00	.158657+01 .623876+00	.143813+01 .683551+00	.129522+01 .705740+00
.60	.229885+01 .0	.211791+01 .559713+00	.170349+01 .878536+00	.148357+01 .930808+00	.128502+01 .927798+00
.70	.273870+01 .0	.243899+01 .813903+00	.179848+01 .119994+01	.148800+01 .122283+01	.122814+01 .117142+01
.80	.330386+01 .0	.281529+01 .116807+01	.185201+01 .159889+01	.143293+01 .155787+01	.111267+01 .142738+01
.90	.403928+01 .0	.325121+01 .166206+01	.183636+01 .208415+01	.129634+01 .192846+01	.927639+00 .168134+01
1.00	.500898+01 .0	.374645+01 .235168+01	.171377+01 .265934+01	.105379+01 .231879+01	.665017+00 .191326+01
1.10	.630524+01 .0	.429102+01 .331474+01	.143482+01 .331817+01	.680682+00 .270192+01	.322278+00 .209753+01
1.20	.806285+01 .0	.485657+01 .465908+01	.938062+00 .403754+01	.156290+00 .303701+01	.945930-01 .220410+01
1.30	.104813+02 .0	.538160+01 .653258+01	.151941+00 .476793+01	.530066+00 .326754+01	.568066+00 .220118+01
1.40	.138599+02 .0	.574679+01 .913501+01	-.998816+00 .542135+01	.137052+01 .332164+01	.106664+01 .205955+01
1.50	.186539+02 .0	.573426+01 .127298+02	-.257974+01 .585743+01	.232809+01 .311621+01	.154400+01 .175882+01
1.60	.255657+02 .0	.496175+01 .176520+02	-.462254+01 .587039+01	.332543+01 .256681+01	.194085+01 .129487+01
1.70	.356950+02 .0	.277771+01 .243017+02	-.708673+01 .518191+01	-.423536+01 .160541+01	.219057+01 .687583+00
1.80	.507889+02 .0	-.190182+01 .331040+02	-.980423+01 .344908+01	-.487786+01 .206798+00	.222934+01 .131466-01
1.90	.736656+02 .0	-.108404+02 .443947+02	-.124081+02 .301777+00	-.502963+01 .157716+01	.201049+01 .725740+00
2.00	.108941+03 .0	-.268411+02 .581561+02	-.142543+02 .457095+01	-.445375+01 .358054+01	.152134+01 .134236+01
2.10	.164294+03 .0	-.542404+02 .734660+02	-.143607+02 .-112629+02	-.295578+01 .-549415+01	.798885+00 .-174372+01
2.20	.252703+03 .0	-.995202+02 .874162+02	-.114096+02 .-194032+02	-.468263+00 .-686146+01	.610500-01 .-182367+01
2.30	.396460+03 .0	-.171913+03 .930880+02	-.389141+01 .-278220+02	.284504+01 .-712231+01	.907518+00 .-152069+01
2.40	.634378+03 .0	-.283609+03 .759226+02	-.950566+01 .-341808+02	.649023+01 .-572745+01	.155613+01 .-849408+00
2.50	.103581+04 .0	-.448599+03 .748935+01	.291411+02 .-347103+02	.959591+01 .-233541+01	.183009+01 .-787847-01
2.60	.172508+04 .0	-.677955+03 .-164667+03	.532363+02 .-243320+02	.109818+02 .-292473+01	.161505+01 .-105855+01
2.70	.293054+04 .0	-.967019+03 .-532419+03	.763516+02 .-239913+01	.941085+01 .-919036+01	.913632+00 .-182663+01
2.80	.508022+04 .0	-.126560+04 .-124780+04	.879744+02 .-489857+02	.405857+01 .-147289+02	.121594+00 .-213210+01
2.90	.898334+04 .0	-.141486+04 .-254465+04	.722456+02 .-112885+03	-.485116+01 .-171054+02	.119568+01 .-182716+01
3.00	.162060+05 .0	-.102319+04 .-474402+04	.105895+02 .-179798+03	-.154399+02 .-138266+02	-.196121+01 .-948998+00
3.50	.417962+06 .0	.759689+05 .-127565+05	-.345002+03 .-846681+03	.352504+02 .-318118+02	.178275+01 .-513342+00
4.00	.177722+08 .0	-.303148+06 .-206132+07	.165184+04 .-572854+04	.-121850+03 .-315751+02	.-201785+01 .-479428+00
4.50	.124593+10 .0	-.632047+08 .-532606+08	.127488+05 .-482630+05	.286262+03 .-246430+03	.248394+00 .-205738+01
5.00	.1144010+12 .0	.504457+10 .-335304+09	-.505861+06 .-179234+06	.714413+03 .-107588+04	.190113+01 .-186596+00
5.50	.274434+14 .0	.398070+12 .-262492+12	.359254+07 .-647923+07	-.294447+04 .-407345+04	.714128+00 .-176703+01
6.00	.862246+16 .0	.457872+14 .-520744+14	.127587+09 .-310891+08	-.217456+05 .-476709+04	.-323300+00 .-191803+01
6.50	.446655+19 .0	-.100716+17 .-118452+17	.133025+10 .-267648+10	-.112172+06 .-340422+04	-.383674+00 .-191335+01
7.00	.381469+22 .0	.433489+19 .-317887+19	.207375+10 .-873217+11	-.630212+06 .-132005+06	.543630+00 .-185111+01
7.50	.537149+25 .0	-.283374+22 .-426347+21	.630673+11 .-327704+13	-.252634+07 .-336114+07	.185781+01 .-535787+00
8.00	.124703+29 .0	.196497+25 .-129886+25	.683728+14 .-142358+15	.165524+08 .-265076+08	.733467+00 .-188952+01
8.50	.477316+32 .0	-.989764+25 .-298524+28	.943832+16 .-252614+16	.206701+09 .-164806+09	-.204721+01 .-598650-01
9.00	.301219+36 .0	-.549838+31 .-194934+31	.397576+18 .-666613+18	-.243169+10 .-751742+09	.150878+01 .-121573+01

## EXP(Z\*\*2)\*ERFC(-Z)

RHO\THETA	50°	60°	70°	80°	90°	
.00	.100000+01	.000000	.100000+01	.000000	.100000+01	.000000
.02	.101443+01	.176847-01	.101108+01	.198904-01	.100741+01	.214606-01
.04	.102869+01	.361748-01	.102172+01	.404727-01	.101417+01	.434163-01
.06	.104275+01	.554874-01	.103189+01	.617442-01	.102026+01	.658462-01
.08	.105656+01	.756385-01	.104154+01	.837004-01	.102564+01	.887273-01
.10	.107009+01	.966430-01	.105064+01	.106335+00	.103029+01	.112035+00
.12	.108331+01	.118515+00	.105916+01	.129639+00	.103418+01	.135743+00
.14	.109617+01	.141267+00	.106704+01	.153603+00	.103728+01	.159822+00
.16	.110862+01	.164910+00	.107424+01	.178212+00	.103956+01	.184242+00
.18	.112062+01	.189453+00	.108074+01	.203453+00	.104100+01	.208971+00
.20	.113213+01	.214906+00	.108648+01	.229307+00	.104157+01	.233974+00
.30	.118204+01	.355926+00	.110242+01	.366982+00	.103071+01	.361797+00
.40	.120806+01	.519531+00	.109341+01	.515837+00	.995593+00	.490450+00
.50	.120731+01	.703662+00	.105496+01	.670616+00	.935432+00	.614113+00
.60	.116980+01	.903774+00	.983747+00	.824347+00	.851095+00	.726620+00
.70	.108743+01	.111228+01	.878285+00	.968587+00	.745231+00	.821976+00
.80	.953336+00	.131817+01	.739549+00	.109394+01	.622230+00	.894945+00
.90	.763292+00	.150697+01	.571471+00	.119083+01	.487972+00	.941619+00
1.00	.517275+00	.166123+01	.381152+00	.125055+01	.349369+00	.959889+00
1.10	.221086+00	.176167+01	.178694+00	.126642+01	.213743+00	.949748+00
1.20	-.112292+00	.178923+01	-.234440-01	.123493+01	.881139-01	.913353+00
1.30	-.462011+00	.172780+01	-.211562+00	.115668+01	-.215044-01	.854822+00
1.40	-.799794+00	.156770+01	-.372237+00	.103688+01	-.110704+00	.779790+00
1.50	-.109192+01	.130926+01	-.494065+00	.688519+00	-.177075+00	.694764+00
1.60	-.130302+01	.965812+00	-.569332+00	.714952+00	-.220337+00	.606395+00
1.70	-.140154+01	.565275+00	-.595323+00	.541594+00	-.242190+00	.520751+00
1.80	-.136640+01	.149190+00	-.574932+00	.380624+00	-.245914+00	.442725+00
1.90	-.119347+01	.231426+00	-.516381+00	.245402+00	-.235801+00	.375650+00
2.00	-.900424+00	.523642+00	-.432005+00	.145177+00	-.216510+00	.321167+00
2.10	-.527958+00	.682837+00	-.336258+00	.837718-01	-.192467+00	.279344+00
2.20	-.135761+00	.683750+00	-.243313+00	.592582-01	-.167392+00	.248996+00
2.30	.207215+00	.529536+00	-.164751+00	.647151-01	-.144014+00	.228112+00
2.40	.437243+00	-.255605+00	-.107845+00	.899283-01	-.123586+00	.214327+00
2.50	.512073+00	.744257-01	-.748106-01	.123641+00	-.107586+00	.205321+00
2.60	.424377+00	.381557+00	-.631827-01	.155822+00	-.959278-01	.199114+00
2.70	.207358+00	.591072+00	-.671444-01	.179408+00	-.872383-01	.194224+00
2.80	-.711724-01	.654101+00	-.794229-01	.191148+00	-.811203-01	.189696+00
2.90	-.326684+00	.563991+00	-.932090-01	.191421+00	-.767654-01	.185036+00
3.00	-.483674+00	.360592+00	-.103604+00	.183219+00	-.734511-01	.180089+00
3.50	.999905-01	.472332-02	-.891007-01	.134728+00	-.617122-01	.154611+00
4.00	-.218410+00	.993987-01	-.749050-01	.122386+00	-.525086-01	.134600+00
4.50	-.558352-01	.147044+00	-.658583-01	.108279+00	-.458045-01	.119295+00
5.00	-.517307-01	.724167-01	-.587417-01	.975944-01	-.406890-01	.107125+00
5.50	-.679421-01	.672066-01	-.530230-01	.887586-01	-.366399-01	.972205-01
6.00	-.639612-01	.683196-01	-.483467-01	.813834-01	-.333477-01	.890010-01
6.50	-.576053-01	.65C358-01	-.444434-01	.751362-01	-.306137-01	.820692-01
7.00	-.526816-01	.605424-01	-.411335-01	.697775-01	-.283042-01	.761436-01
7.50	-.488796-01	.571703-01	-.382898-01	.651309-01	-.263257-01	.710192-01
8.00	-.457747-01	.537426-01	-.358190-01	.610637-01	-.246107-01	.665434-01
8.50	-.430626-01	.506142-01	-.336516-01	.574741-01	-.231091-01	.626001-01
9.00	-.406279-01	.478200-01	-.317343-01	.542828-01	-.217828-01	.590993-01